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Tables

**Table 1-1. Summary of Supporting Investigations and Reports**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| <b>Timeframe of Relevant Activity/ Investigation</b> | <b>Report Title</b>   | <b>Author(s)</b>            | <b>Entity Responsible</b> | <b>Report Year</b> | <b>Reference Location</b>            |
|--|---|-----------------------------|---------------------------|--------------------|--------------------------------------|
| June 1984  | Remedial Investigation of Soils, Vegetation, and Livestock  | CH2M HILL                   | USEPA                     | 1987               | Section 3.2                          |
| Nov 1984 - May 1988                                  | Process Pond Remedial Investigation/Feasibility Study   | Hydrometrics and Hunter/ESE | ASARCO                    | 1989               | Section 3.2                          |
| Fall 1984 - Spring 1988                              | Comprehensive Remedial Investigation/Feasibility Study for the Asarco East Helena Smelter   | Hydrometrics                | ASARCO                    | 1990               | Section 3.2                          |
| 1998-1999  | Current Conditions/Release Assessment, East Helena Facility   | Hydrometrics                | ASARCO                    | 1999               | Section 3.2                          |
| 1984 - 2002  | Phase I RCRA Facility Investigation Site Characterization Report - East Helena Facility   | Hydrometrics                | ASARCO                    | 2005               | Section 3.2                          |
| 2003   | Supplemental Ecological Risk Assessment for the East Helena Smelter Site, Montana   | USEPA                       | USEPA                     | 2005               | Section 2.3.3                        |
| 2009   | U.S. East Helena Superfund Site, Operable Unit No. 2, Residential Soils and Undeveloped Lands, Final Record of Decision                         | USEPA                       | USEPA                     | 2009               | Sections 1.2, 2.3.1, 2.3.3, 3.2.5, 6 |
| 2010   | Phase II RCRA Facility Investigation, East Helena Facility  | GSI Water Solutions, Inc.   | Custodial Trust           | 2014               | Sections 3.2 and 3.3.5               |
| 2010   | Baseline Ecological Risk Assessment: Former ASARCO East Helena Facility, East Helena, Montana   | Gradient                    | Custodial Trust           | 2011               | Section 3.4.2                        |
| 2011   | Preliminary Evaluation of South Plant Hydraulic Control at the East Helena Smelter Facility   | GSI Water Solutions, Inc.   | Custodial Trust           | 2011               | Section 3.3.2                        |
| 2011-2012  | Draft Upper Lake Drawdown Test Technical Memorandum   | Hydrometrics, Inc.          | Custodial Trust           | 2012               | Sections 3.3.2 and 5.2               |
| 2012   | Former ASARCO East Helena Facility Interim Measures Work Plan - Conceptual Overview of Proposed Interim Measures and Details of 2012 Activities | CH2M HILL                   | Custodial Trust           | 2012               | Section 5                            |
| 2013   | Former ASARCO East Helena Facility Interim Measures Work Plan – 2013  | CH2M HILL                   | Custodial Trust           | 2013               | Section 5.3                          |
| 2014   | Former ASARCO East Helena Facility Interim Measures Work Plan – 2014  | CH2M HILL                   | Custodial Trust           | 2014               | Section 5.3                          |
| 2014   | 2014 Supplemental Contaminant Source Area Investigation at the Former East Helena Smelter   | Hydrometrics, Inc.          | Custodial Trust           | 2015               | Section 3.3.5                        |
| 2014   | Groundwater Flow Model Calibration Refinement, Transient Verification, and Interim Measures Support, East Helena Site                           | NewFields                   | Custodial Trust           | 2014               | Section 5                            |
| 2014-2015  | Groundwater Remedy Evaluation and Recommendations for the Former East Helena Smelter  | CH2M HILL                   | Custodial Trust           | 2016               | Sections 3.3.5 and 5                 |
| 2015   | Former ASARCO East Helena Facility Corrective Measures Study Work Plan  | CH2M                        | Custodial Trust           | 2015               | Sections 3.3.4, 3.3.5, and 3.4.2     |
| 2015   | 2015 Groundwater and Surface Water Corrective Action Monitoring Plan, East Helena Facility  | Hydrometrics, Inc.          | Custodial Trust           | 2015               | Section 3.3.1 and 5                  |
| 2015   | Final Fate and Transport Model Design and Calibration, East Helena Site   | NewFields                   | Custodial Trust           | 2015               | Section 5                            |
| 2015   | Basis of Design Report for the ET Cover System, Interim Cover System 2, and Demolition Phase 3  | CH2M HILL                   | Custodial Trust           | 2015               | Section 5.3                          |
| 2015   | 2015 Supplemental Contaminant Source Area Investigation at the Former East Helena Smelter   | Hydrometrics, Inc.          | Custodial Trust           | 2016               | Sections 3.3.5 and 5                 |
| 2015-2016  | Former ASARCO East Helena Facility Interim Measures Work Plan – 2015 and 2016   | CH2M HILL                   | Custodial Trust           | 2015               | Section 5.3                          |
| 2015-2016  | East Helena Facility Supplemental RFI Sampling and Analysis Plan  | CH2M HILL                   | Custodial Trust           | 2015               | Section 3.3.4                        |
| 2015-2016  | Addendum to Former ASARCO East Helena Facility Interim Measures Work Plan – 2015 and 2016   | CH2M HILL                   | Custodial Trust           | 2016               | Section 5.3                          |
| January - March 2016                                 | 2016 Speiss/Dross Slurry Wall Evaluation Technical Memorandum   | Hydrometrics, Inc.          | Custodial Trust           | 2016               | Section 3.3.5                        |
| 2016   | Addendum to East Helena Facility Supplemental RFI Sampling and Analysis Plan  | CH2M                        | Custodial Trust           | 2016               | Section 3.3.4                        |
| 2016   | 2016 Groundwater and Surface Water Corrective Action Monitoring Plan, East Helena Facility  | Hydrometrics, Inc.          | Custodial Trust           | 2016               | Section 3.3.1                        |
| 2016   | Existing Information and Data Compilation for the Former East Helena Smelter Slag Pile Area Technical Memorandum                                | Hydrometrics, Inc.          | Custodial Trust           | 2016               | Section 3.3.6                        |

Notes:

ASARCO = American Smelting and Refining Company

RCRA = Resource Conservation and Recovery Act

RFI = RCRA Facility Investigation

USEPA = U.S. Environmental Protection Agency

**Table 2-1. CMS Parcels - Media Cleanup Standards for Primary Inorganic Constituents in Soil**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Media         | Constituent of Potential Concern | Land Use                | Cleanup Standard (µg/L groundwater, mg/kg soil) <sup>d</sup> | Basis of Standard  | Applications for Standard  |
|---------------|----------------------------------|-------------------------|--|--|--|
| Groundwater   | Arsenic                          | All                     | 0.010  | MCL  | Exceedance of MCS indicates need for remedial action and will be considered in identification of areal extent of institutional controls (Controlled Groundwater Area)                                    |
|               | Cadmium                          |                         | 0.005  |  |  |
|               | Selenium                         |                         | 0.05   |  |  |
| Surface Soil  | Lead                             | Ecological              | 650  | Concentration established to be protective of ecological receptors (passerines) at other MT remediation sites <sup>a</sup> | Will be applied as a design criterion for IM and final remedy construction (final surface site work associated with Prickly Pear Creek and Tito Park excavation, surface layer of ET Cover System, etc.) |
|               |                                  | Residential             | 400  | USEPA RSL <sup>b</sup>   |  |
|               |                                  | Industrial - Commercial | 800  |  |  |
|               |                                  | Recreational            | 3,245  | OU-2 ROD   |  |
|               | Arsenic                          | Residential             | 35   | Hegeler Zinc ROD <sup>c</sup>  | Establishes concentration threshold for remedy implementation on undeveloped properties when land use changes  |
|               |                                  | Industrial - Commercial | 572  | OU-2 ROD   |  |
|               |                                  | Recreational            | 794  | OU-2 ROD   |  |
|               |                                  |                         |  |  |  |
| Soil at Depth | Arsenic                          |                         | 40   | (MDEQ, 2013)   | Establishes extent of remedial action required to prevent groundwater contact with contaminated soil and to control infiltration   |
|               | Cadmium                          |                         | 0.38   | USEPA MCL-based SSL <sup>b</sup> (concentration needed to achieve MCLs in groundwater)                                     |  |
|               | Selenium                         |                         | 0.26   | USEPA MCL-based SSL <sup>b</sup> (concentration needed to achieve MCLs in groundwater)                                     |  |

<sup>a</sup> Recommended based on its consistency with action levels developed at other similar smelter/mining sites: OU2 Record of Decision (ROD) East Helena, MT; Anaconda Smelter Superfund Site, Anaconda, MT; Bunker Hill Superfund Site, Coeur d'Alene, ID; and Tri-State Mining District (Oklahoma, Kansas, and Missouri) Superfund Site.

<sup>b</sup> USEPA June 2015 RSL or MCL-based soil screening level (SSL) where indicated

<sup>c</sup> The arsenic cleanup level is recommended based on risk-based concentrations currently being approved by USEPA at former smelter sites and similar facilities across the country. The Hegeler Zinc ROD is cited as an example of current practice (USEPA, 2014).

<sup>d</sup> Media cleanup standards for CMS Parcels as presented in the CMS Workplan (EPA Approval, October 22, 2015); OU-2 ROD standards will be applied to the Undeveloped Lands.

Abbreviations:

- µg/L = micrograms per liter
- ET = evapotranspiration
- IM = interim measure
- MCL = maximum contaminant level
- MDEQ = Montana Department of Environmental Quality
- mg/kg = milligrams per kilogram
- OU2 ROD = Record of Decision for Operable Unit 2
- RSL = regional screening level

**Table 3-1. Summary of Interim Measures Completed by ASARCO**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| <b>Approximate Dates</b>   | <b>Summary of Interim Measure</b>  |
|--|--|
| <b>Sediment and Surface Water (Diversions/Modifications/Management):</b> |  |
| 1996-1997  | Surface water:<br>1996: Switch to use of water from Upper Lake rather than Lower Lake for dust control<br>1997: Wilson Ditch rerouted around plant site<br>1997: Improve plant stormwater system   |
| 1986-1991  | Thornock Lake Removal – key items as follows:<br>1986-1987: soil excavated from Thornock Lake area.<br>1986: Thornock Lake replaced with 93,000 gallon steel tank<br>1991: 407 CY of soil excavated from former Thornock Lake and smelted  |
| 1989-1996  | Lower Lake Dredging/Water Treatment Plant – key items as follows:<br>1989: Bench-scale testing for the treatment of Lower Lake water<br>1990: Discontinue regular discharge of plant water to Lower Lake (occasional discharge from tanks when needed).<br>1993: Begin construction of high-density sludge water treatment plant<br>1993: large-scale dredging and dewatering pilot testing of Lower Lake sediments<br>1994: HDS water-treatment plant comes on-line; discharges to Lower Lake cease<br>1994-1996: dredging of Lower Lake sediments<br>1996: MPDES permit issued for HDS plant discharge |
| <b>Surface Soil and Demolition of the Ore Storage Area:</b>              |  |
| 1989   | Shallow soil removed and stored in Lower Ore Storage Area, deeper soil consolidated in southeast corner of the storage yard  |
| 1997   | Geomembrane cover is installed over stockpiled Lower Lake sediments as a temporary cover   |
| 2000   | Construct Phase I CAMU for waste management  |
| 2009   | Demolished process unit smelter stacks   |
| <b>Former Speiss Settling Pond and Granulating Pit:</b>                  |  |
| 1988   | Speiss Pond lined with high-density polyethylene   |
| 1989   | Replace Speiss pond with settling tank and secondary leak detection  |
| 1989   | 2,500 CY soil excavated to 20 feet under former Speiss Pond  |
| 1991   | Discontinue water granulation of Speiss  |
| 1992   | Demolish Speiss pond and excavate soil   |
| 1993   | Cap former Speiss pond area with concrete.   |
| 1995   | Excavate and cap (concrete) former Speiss pit to 17-foot depth (235 CY removed)  |
| 2006-2007  | Construct slurry wall and cap around Speiss-dross plant subsurface soil.   |
| <b>Acid Plant Water:</b>   |  |
| 1991   | Eliminated wooden trough fluid transport system and settling dumpsters, reducing water losses.   |
| 1992   | Complete water reclamation facility and discontinue use of sediment drying pad   |
| 1993   | Demolish and excavate Acid plant settling pond   |
| 1997   | Re-brick acid plant scrubber sump and install secondary containment  |
| <b>Acid Plant Sediment Drying Area:</b>                                  |  |
| 1991   | Remove Acid plant sediments from former sediment drying pad  |
| 1993   | Seal Former acid plant sediment drying pad   |
| 2001   | Soil and debris stockpiles from remedial actions placed in the CAMU 1  |
| 2006   | Construct slurry wall and cap around APSD subsurface soil  |

**Table 3-2. Summary of Remediation Waste Generation and Management During Interim Measure Implementation**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Remedial Activity                          | Waste Source Area  | Waste Type(s)  | Dates of Removal | Waste Disposal  |                  |
|--|--|--|------------------|---|------------------|
|  |  |  |                  | Location  | Waste Quantities |
| <b>ASARCO-Implemented Interim Measures</b> |  |  |                  |   |                  |
| Lower Lake Sediment Dredging               | Lower Lake   | Sediment   | 1994-1996        | Temporarily stockpiled in Lower Ore Storage Area. Placed in CAMU 1 in 2001. | 27,000 cy        |
|  |  |  |                  | Smelted   | 4,000 cy         |
| Thornock Lake Removal                      | Thornock Lake  | Sediment   | 1986-1987        | Smelted   | Not Provided     |
|  | Thornock Lake  | Sediment   | 1991             | Smelted   | 407 cy           |
|  |  | Slag   | 1991             | Placed on slag pile   | 185 cy           |
| Speiss/Dross Area Removal                  | Speiss Pond  | Soil   | 1988             | Smelted   | 2,500 cy         |
|  | Speiss Pond  | Soil   | 1992             | Temporarily stockpiled in Lower Ore Storage Area. Placed in CAMU 1 in 2001. | 235 cy           |
|  | Speiss Pond  | Soil   | 1995             | Temporarily stockpiled in Lower Ore Storage Area. Placed in CAMU 1 in 2001. | 250 cy           |
| Acid Plant Removal                         | Acid Plant Settling Pond   | Soil   | 1993             | Temporarily stockpiled in Lower Ore Storage Area. Placed in CAMU 1 in 2001. | 2,200 cy         |
|  | Former Sediment Drying Pad   | Sediment   | 1991             | Smelted   | Not Provided     |
|  | Original Sediment Drying Pad   | Soil/Sediment  | 1993             | Temporarily stockpiled in Lower Ore Storage Area. Placed in CAMU 1 in 2001. | Not Provided     |
| Stockpile Removal                          | Lower Ore Storage Area, Shew Ridge, Lower Lake Sediment Stockpile, and Tito Park Area Stockpiles | Soil/Sediment/Debris   | 2001             | CAMU 1  | 110,000 cy       |
| 2008 Facility Demolition                   | Site Structures (Process and Nonprocess) <sup>a</sup>  | Building Debris (wood, brick, insulation, concrete, pipe, other cleanup waste) | 2008             | CAMU 2  | 37,471 cy        |

**Table 3-2. Summary of Remediation Waste Generation and Management During Interim Measure Implementation**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Remedial Activity                                   | Waste Source Area                                     | Waste Type(s)   | Dates of Removal                    | Waste Disposal                       |                      |
|---|---|---|-------------------------------------|--------------------------------------|----------------------|
|   |   |   |                                     | Location                             | Waste Quantities     |
| 2009 Facility Demolition                            | Site Structures (Process and Nonprocess) <sup>b</sup> | Building Debris (wood, brick, insulation, concrete, pipe, building cleaning, other cleanup waste)<br>Yard Debris (railroad ties, roadway sweepings) | 2009                                | CAMU 2                               | 18,565 cy            |
| <b>Custodial Trust-Implemented Interim Measures</b> |   |   |                                     |                                      |                      |
| Phase 1 Demolition                                  | Site Structures (Nonprocess) <sup>c</sup>             | Metal   | 4/2013 - 7/2013                     | Offsite                              | 2,176 tons           |
| Phase 2 Demolition                                  | Site Structures (Nonprocess) <sup>d</sup>             | Metal   | 7/2013 - 10/2013                    | Offsite                              | 1,249 tons           |
|   | Site Structures (Nonprocess) <sup>e</sup>             | Building Debris (wood, brick, insulation, concrete, pipe)<br>Yard Debris (dirt, fabrics, railroad ties, miscellaneous)                              | 9/2013 - 10/2013                    | CAMU 2                               | 2,618 tons           |
| Tito Park Area Removal                              | Acid Plant Sediment Drying Area/<br>Tito Park Area    | Slurry Wall Material,<br>Speiss, Contaminated Soil, Sand,<br>Rusted/Crushed Ore Barrels, Concrete   | 7/2014 - 8/2014                     | CAMU 2                               | 30,270 cy            |
|   | Tito Park Area  | Lower Lake Sediments,<br>Contaminated Soil, Other Soil  | 6/2014 - 9/2014                     | ET Cover West<br>Subgrade            | 150,000 cy           |
| PPC Realignment                                     | Upper Lake Marsh                                      | Contaminated Marsh Sediments  | 9/2016 - 10/2016                    | ET Cover East<br>Subgrade            | 21,000 cy            |
| Phase 3 Demolition                                  | Site Structures (Process) <sup>c</sup>                | Construction and Debris,<br>Universal Wastes,<br>Refrigerants   | 6/2015 - 8/2016                     | Offsite                              | 1,400 tons           |
|   | Speiss Disposal                                       | Metal<br>Speiss; Contaminated Soil  | 6/2015 - 10/2016<br>7/2016 - 9/2016 | Offsite<br>ET Cover East<br>Subgrade | 756 tons<br>8,000 cy |
| Acid Plant Removal                                  | Acid Plant Settling Pond                              | Contaminated Soil; Concrete   | 4/2016 - 8/2016                     | ET Cover East<br>Subgrade            | 20,000 cy            |

<sup>a</sup> Primary structures included: Acid Plant, Bag House, Bailey Building Stored Waste, Barnum Building Stored Waste, Ore Storage Stored Waste, Ringling Building, Spray Dryer, Blast Furnace Flue, Monier Flue

<sup>b</sup> Primary structures included: Acid Dust Silo, Crushing Mill, Sample Mill, Hopto Pad, Breaking Floor/Highline, Ore Storage RR Track Area, Ore Storage Walls Demolition, 200-foot Stack, 400-foot Stack, 425-foot Stack, Ore Storage Cleaning, Ore Storage Baghouse Cleaning, Ore Storage Sump Cleaning, Crushing Mill Cleaning, Sample Mill Cleaning, Hopto Pad Cleaning, Bailey Building Cleaning, Cement Silo Cleaning, Coke Hopper Cleaning, Direct Smelt Building Cleaning, High Grade Cleaning, Scale House Cleaning, Water Treatment Plant Sump Cleaning, Sump Near Scale House Cleaning, Sump South of Barnum Cleaning, Debris Around Bailey Building Cleaning, Million-gallon-tank Cleaning

<sup>c</sup> Primary structures included: Ore Storage and Handling, Barum and Bailey Buildings, Scales and Scalehouse

<sup>d</sup> Primary structures included: Powerhouse, Warehouse, Welding Shops, DOES Building, Direct Smelt Building, Zinc Plant O<sub>2</sub> Building, Other miscellaneous structures and debris

<sup>e</sup> Primary structures included: Engineering Building, Bathhouse Building, Stormwater Tanks; HDS Treatment; Transformer Pad Area; Power Building, etc.

Notes:

cy = cubic yards; HDS = high-density sludge

Table 3-3. Former East Helena Smelter Groundwater Contaminant Source Inventory  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| General Source Area     | Source # | Source Name  | Primary COC As/Se | Description  | Soil Conditions   | Groundwater Conditions  | Recommendations  |
|-------------------------|----------|--|-------------------|--|---|---|--|
| West Selenium Area      | 1        | Rail Corridor Soils  | Se                | Rail corridors adjacent to former ore storage building. SPLP leach samples showed 0.027 to 0.490 mg/L selenium. Leachability increased with depth while total concentrations decreased with depth.   | Elevated total Se concentrations in near surface soils decrease with depth. Phase II RFI surface soil samples ranged from 569 to 754 mg/kg at RCSS-5 and RCSS-7 (0-6"), decreased to 13 to 96 mg/kg respectively at 2.5-5 feet. Boring RFI2SB-9 surface (slag) samples showed 151 to 281 mg/kg Se, decreased to <5 mg/kg in deeper samples.   | Seasonal Se spikes up to 7 mg/L (DH-66), appear to have been mitigated by SPHC. "Baseline" concentrations still 1-2 mg/L range, most recent concentrations 4-6 mg/L (2014). Well DH-66 highly correlated with water table variations and other parameters (SO <sub>4</sub> , Cl), DH-8 less so (different mechanisms?). Groundwater saturated with respect to gypsum (CaSO <sub>4</sub> ) and calcite (CaCO <sub>3</sub> ). Low arsenic concentrations in this area. Possible secondary mineral cement source.  | Although they cannot be ruled out due to high leach concentrations, surface soils seem an unlikely source of seasonal spikes in groundwater. Additional data to be collected as part of 2014 source characterization work. Should be addressed through capping.  |
|                         | 2        | Selenium-Loaded Saturated Soils: impacted from Speiss-Dross Area Groundwater | Se                | Not a former process area. Downgradient of historic source areas (speiss/dross and/or acid plant). Selenium historically loaded onto saturated soils via groundwater transport, possibly precipitated or occluded within minerals former in aquifer matrix during mixing/neutralization of acid plant and speiss dross impacted groundwater. May be released over time, with changing geochemical conditions. Process water in speiss/dross reportedly contained ~40 mg/L selenium, acid plant process water ~6 mg/L selenium. Well DH-21 in speiss/dross area reported about 7 mg/L in 1999 as part of plant water release investigation. | Concentrations and leachability of Se in subsurface soils (both saturated and unsaturated) not well documented. Location estimated based on configuration of west selenium plume.   |   | Possible significant source of current selenium loading to groundwater. Evaluate further for possible mitigation. Additional subsurface data needed.   |
|                         | 3        | Selenium-Loaded Saturated Soils: Impacted from Acid Plant Area Groundwater   | Se                | Not a former process area. Downgradient of historic source area (speiss/dross) and slurry wall, upgradient of PRB. Arsenic historically loaded onto saturated soils via groundwater transport from upgradient sources; may be released over time with changing geochemical conditions. Also some potential for Se release based on RFI2SB-20 results (leached 0.7 mg/L Se during adsorption tests) and recent gw trends at well DH-36 (As decrease/Se increase).   | Concentrations and leachability of Se in subsurface soils (both saturated and unsaturated) not well documented. Location estimated based on configuration of west selenium plume.   |   | Possible significant source of current selenium loading to groundwater. Evaluate further for possible mitigation. Additional subsurface data may be needed.  |
| North Plant Source Area | 4        | North Plant Site Saturated Soils   | As (Se?)          | Not a former process area. Downgradient of historic source area (speiss/dross) and slurry wall, upgradient of PRB. Arsenic historically loaded onto saturated soils via groundwater transport from upgradient sources; may be released over time with changing geochemical conditions. Also some potential for Se release based on RFI2SB-20 results (leached 0.7 mg/L Se during adsorption tests) and recent gw trends at well DH-36 (As decrease/Se increase).   | Organic contamination at water table common in wells and soil borings. Deep (saturated) soil As concentrations highest at DH-13 (300-1400 mg/kg), DH-17 (300-700 mg/kg). More recent data somewhat lower: Phase II RFI borings in area range from 25-432 mg/kg; lower on As plume periphery. As adsorption observed at RFI2SB-8 and -21. As leaching at RFI2SB-16 (40-42'), adsorption at 25-32'.   | Downgradient of slurry wall, gw concentrations are 3-12 mg/L range (SDMW-1, -2, -5, DH-13). 450' downgradient at DH-17 concentrations are 35 mg/L. DH-17 concentrations stable since 2002 but have recently decreased to minimum seen since 2002 (from 45 mg/L down to 31.5 mg/L). As(III) predominant at DH-17, continuing downgradient to DH-64, alters to As (V) as plume crosses Highway 12.  | Possible primary current source of arsenic loading to downgradient groundwater. Potential future source of selenium loading to groundwater if geochemical conditions change. Evaluate further for possible mitigation. Additional subsurface data needed.  |
| Slag Pile               | 5        | Younger Unfumed Slag   | As/Se             | Slag not processed through zinc plant during periods prior to zinc plant construction (1930s) and following cessation of zinc plant operation (1982). Generally south end and "upper lift" of slag pile.   | Unfumed slag shows higher total metals concentrations than fumed slag. Phase II RFI samples from well DH-74 showed 97 to 209 mg/kg Se and 814 to 1840 mg/kg As from 0-42 feet; deeper samples showed <5 to 17 mg/kg Se and 9 to 194 mg/kg As. Slag leach concentrations from Phase II RFI (SPLP) showed 0.009 to 0.130 mg/L As, 0.036 to 0.400 mg/L Se. RI/FS era slag leach and test basin samples showed 0.353 to 0.620 mg/L As in test basins and 0.31 mg/L As in bottle roll for unfumed slag. Fumed slag showed lower concentrations (0.0283 to 0.054 mg/L in test basins and 0.19 mg/L in bottle roll). Test basin K results were 54 to 74 mg/L for fumed slag, 1540 to 2650 mg/L for unfumed slag. Bottle roll K results were 3.9 mg/L for fumed and 22 mg/L for unfumed slag. | Selenium and arsenic concentrations in area currently highest near north and northwest portion of slag pile. Highest Se concentrations at well DH-56. Some Se (IV) contribution in this area. Very high K concentrations at DH-56 (400 mg/L). As about 1-2 mg/L and Se 0.4 to 1.0 mg/L in select wells, some wells lower. South of well DH-55 Se is below detect, As about 0.3 mg/L. Groundwater beneath south portion of pile appears more reducing due to influence of marsh sediments. Alluvial aquifer beneath slag pile shows downward vertical gradient and decreasing concentrations with depth; possible indication of loading from above (slag). Although lower concentration, selenium originating from slag pile area a significant source of downgradient selenium loading due to greater groundwater flux. | Large area and not well defined as a whole. Review of slag pile history (available analytical data, aerial photo and map review to determine placement of slag over time, field reconnaissance) recommended to evaluate potential areas of contaminant loading from slag; possible more detailed evaluation in future if warranted. Not a time critical source area relative to near-term remedial activities. |

Table 3-3. Former East Helena Smelter Groundwater Contaminant Source Inventory  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| General Source Area      | Source # | Source Name                      | Primary COC As/Se | Description  | Soil Conditions  | Groundwater Conditions  | Recommendations  |
|--------------------------|----------|----------------------------------|-------------------|--|--|---|--|
| Former Thornock Lake     | 6        | Former Thornock Lake Area Soils  | As                | Former process pond. Pond replaced with tank in 1986. Soils excavated in 1986-1987 and 1991.   | Preremediation total As in soils as high as 120,000 mg/kg but quite variable. Post-excavation samples in 1991 showed total As 513 to 3055 mg/kg. SPLP As 0.22 to 3.8 mg/L. SPLP Se all <0.1 mg/L. Phase I RFI soil borings RFISB-1 and RFISB-2 showed relatively low total arsenic concentrations (<10 to 231 mg/kg, average of 32 mg/kg).   | Groundwater at wells DH-57 in DH-58 in Thornock Lake area recently 1-2 mg/L arsenic, 0.01 to 0.05 mg/L selenium. Generally decreasing trends since plant shutdown.  | Not associated with highest GW concentrations although some leachable arsenic probably remains in soils. Further consideration not warranted at this time given the other areas with much higher impacts to groundwater. May warrant further evaluation some time in the future depending on water quality trends and project developments.  |
| Former Speiss/Dross Area | 7        | Speiss Granulation Area          | As/Se             | Very high historic process water concentrations for both arsenic (3,000+ mg/L) and selenium (40+ mg/L). Historic area of highest groundwater impacts due to use of ponds, process water releases. Elevated groundwater pH (11-13). Encapsulated in slurry wall in 2007; slurry wall appears effective at limiting downgradient migration of contaminants (As at SDMW-2 decrease of 50+mg/L to 10 mg/L since 2007). | Variable due to historic soil removal actions. Likely still some areas of elevated soil arsenic concentrations, particularly within saturated zone. Selenium concentrations unknown within wall. Phase I RFI soil borings RFISB-3 and RFISB-4 showed moderate arsenic soil concentrations (<10 to 777 mg/kg, average of 243 mg/kg). Phase II boring north of wall (RFI2SB-20) leached up to 0.7 mg/L Se from sample with total Se of 17 mg/kg. | Groundwater arsenic as high as 750 mg/L in the past, selenium as high as 7 mg/L but very limited data (well DH-21). Current arsenic concentrations within slurry wall 80 to 100 mg/L. Groundwater yield within wall appears to be decreasing over time. | Groundwater quality generally improving in area. May warrant further evaluation in future depending on water quality trends within and outside of slurry wall, and long-term integrity of wall. Potential source areas outside of slurry wall should be evaluated as potential source to West Selenium Area groundwater plume. Not a time critical source.   |
|                          | 8        | Speiss Storage and Handling Area | As/Se             | Outside storage bins and material handling area for speiss. Likely impacts from material spillage and water application. Partially encapsulated in slurry wall in 2007; slurry wall appears effective at limiting downgradient migration of contaminants. Portion outside (west) of slurry wall.   | Limited soil data in this area. Well DH-38 soil samples showed 72 to 1906 mg/kg total arsenic. Concentrations increased from about 170 mg/kg just above water table to 700 mg/kg just below water table.   | Arsenic concentrations up to 250 mg/L historically in groundwater at well DH-38. No recent water quality data from area.  | Area outside slurry wall warrants further evaluation as potential source to West Selenium Plume area. Majority of high concentration soils within slurry wall, and limited downgradient migration of arsenic currently indicated. Long-term integrity of slurry wall should be evaluated.  |
| Former Acid Plant Area   | 9        | Cottrell/Scrubber Blowdown Area  | As/Se             | Area of significant process water leaks during plant operations; very high process water concentrations (1,800 mg/L As; 5 mg/L Se; 200 mg/L Cd). Extensive remediation conducted in Acid Plant Area in late 1980s/early 90s. Contaminated soils remain at depth at location of former acid plant settling pond and possibly other areas.   | Soils highly impacted by historic process water releases; highest concentration soils excavated in 1990s. Current concentrations up to 12,000 mg/kg arsenic at former settling pond area. Highest concentration soils recently desaturated by SPHC IM. High concentration soils are localized and located under high-density sludge building.  | DH-19 up to 416 mg/L arsenic in groundwater in 1991. Arsenic concentrations have decreased from about 11.5 to 9 mg/L since 2011. Selenium decrease recently from 60 to 25 ppb. Recent improvements attributed to SPHC.                                  | Historically significant source of arsenic loading to groundwater, but groundwater quality improving due to past remedial activities and recent SPHC IM. Localized high arsenic concentration soils at former Acid Plant Settling Pond may warrant removal or other source control after high-density sludge demolition and before capping in late 2016. Monitor groundwater level and quality trends through 2015 to determine full response to SPHC, and select course of action for 2016. |
|                          | 10       | Acid Plant Settling Pond         | As/Se             |  |  |   |  |
|                          | 11       | Original AP Sediment Drying Area | As/Se             |  |  |   |  |
| Monier Flue              | 12       | Monier Flue Area Soils           | Se                | Soils beneath former Monier Flue, which was removed in 2008, are largely unsaturated. Potential contaminant mechanism was periodic washing out of flue with water and letting water infiltrate into ground. Soils sampled during demolition and during Phase II RFI.   | Demolition soil samples up to 1,350 mg/kg selenium; highest document soil concentration. Phase II boring RFISB-6 up to 106 mg/kg at 2 to 5 feet; leached 0.28 mg/L. Very high cadmium (75,000 mg/kg), lead (53,000 mg/kg), copper (17,000 mg/kg). All concentrations decreased significantly below 5 feet bgs.   | No data; aquifer very thin (2 to 0 feet thick).   | Underlying soils dry down to clay layer in most areas; elevated selenium soils will be addressed through capping. No need to evaluate further.   |



Table 3-3. Former East Helena Smelter Groundwater Contaminant Source Inventory  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| General Source Area | Source # | Source Name                    | Primary COC As/Se | Description   | Soil Conditions  | Groundwater Conditions | Recommendations  |
|---------------------|----------|--------------------------------|-------------------|---|--|------------------------|--|
| South Plant         | 13       | Upper Ore Storage Area         | As/Se             | Area used for storage of ore and other materials historically.  | NA -- draining of Lower Lake and removal of soils to 3910 feet amsl in Tito Park/APSD/UOS areas conducted as part of TPA Source Removal/SPHC IM projects. Post-SPHC conditions to be determined. |                        | To be addressed through TPA Source Removal and SPHC IMs. |
|                     | 14       | Former AP Sediment Drying Area | As                | Former acid plant sediment drying area associated with elevated groundwater arsenic and metals concentrations, along with elevated soil concentrations. Encapsulated in APSD slurry wall in 2006.   |  |                        |  |
|                     | 15       | Lower Lake/Tito Park           | As/Se             | Lower Lake historically used as process pond, more recently as water treatment plant MPDES discharge point. Contaminated sediments dredged from lake in mid-1990s. Tito Park used as storage area for various materials throughout plant history. Materials removed to CAMU in early 2000s. |  |                        |  |

Notes:  
 General source areas are shown on Figure 3-7.  
 AP = Acid Plant Area  
 AS/SE = arsenic/selenium  
 bgs = below ground surface  
 CAMU = Corrective Action Management Unit  
 COC = constituent of concern  
 mg/kg = milligrams per kilogram  
 mg/L = milligram per liter  
 NA = not applicable  
 SD = Speiss/Dross Area  
 SPCH IM = South Plant Hydraulic Control interim measure  
 SPLP = Synthetic Precipitation Leaching Procedure

|  |   |
|--|---|
|  | Recommended for additional evaluation     |
|  | Not recommended for additional evaluation |

**Table 3-4. Overview of 2014 Source Area Investigation and Analyses Completed**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| <b>Source Area</b>  | <b>Number of Borings</b> | <b>Number of Wells Completed</b> | <b>Number of Soil Samples</b> | <b>Summary of Analyses</b>  |
|---------------------|--------------------------|----------------------------------|-------------------------------|---|
| West Selenium       | 6                        | 2                                | 33                            | Soil leach testing<br>Total metals (soil)<br>Arsenic and selenium (groundwater)<br>Mineralogical analysis |
| North Plant Arsenic | 2                        | 0                                | 9                             | Soil leach testing<br>Total metals (soil)<br>Arsenic and selenium (groundwater)<br>Mineralogical analysis |

Note:

Leach Testing = synthetic precipitations leaching procedure and saturated paste analyses.

**Table 3-5. Overview of 2015 Source Area Investigation and Analyses Completed**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Source Area         | Number of Borings | Number of Wells Completed | Number of Soil Samples | Summary of Analyses   |
|---------------------|-------------------|---------------------------|------------------------|---|
| West Selenium       | 7                 | 2                         | 43                     | Soil leach testing<br>Total Metals (soil)<br>Arsenic and selenium (groundwater) |
| North Plant Arsenic | 2                 | 0                         | 16                     | Total metals (soil)<br>Batch adsorption testing                                 |
| Acid Plant          | 4                 | 2                         | 23                     | Soil leach testing<br>Total metals (soil)<br>Arsenic and selenium (groundwater) |
| Speiss-Dross Area   | 2                 | 1                         | 11                     | Soil leach testing<br>Total metals (soil)<br>Arsenic and selenium (groundwater) |

Notes:

Leach Testing = synthetic precipitations leaching procedure and saturated paste analyses.

Intact Shelby tube soil cores were collected for potential geotechnical analysis at seven locations, as follows:

- Five locations in the West Selenium source area
- One location in the former Acid Plant source area
- One location in the Speiss-Dross source area

Table 3-6. Total and Leachate Concentrations (2001 - 2010) for Unfumed and Fumed Slag  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| Slag Type   | Statistic | Total Concentrations in Slag (mg/kg) |             |              |            |               | Slag Leachate Concentrations (mg/L) |              |                                |              |              |           |             |             |             |             |             |           |
|---|-----------|--------------------------------------|-------------|--------------|------------|---------------|-------------------------------------|--------------|--------------------------------|--------------|--------------|-----------|-------------|-------------|-------------|-------------|-------------|-----------|
|   |           | Arsenic                              | Copper      | Lead         | Selenium   | Zinc          | Phase I and II RFI SPLP Samples     |              | RI/FS Slag Infiltration Basins |              |              |           |             |             |             |             |             |           |
|   |           |                                      |             |              |            |               | Arsenic                             | Selenium     | Arsenic                        | Copper       | Lead         | Selenium  | Zinc        | Potassium   | Sodium      | Sulfate     | pH (s.u.)   |           |
| Unfumed Slag (pre-early 1940s deep lift) <sup>a</sup> | Minimum   | 34.1                                 | 75.7        | <10          | 10         | 1600          | 0.099                               | 0.036        | NA                             | NA           | NA           | NA        | NA          | NA          | NA          | NA          | NA          | NA        |
|   | Maximum   | 3060                                 | 54300       | 41600        | 160        | 114000        | 0.099                               | 0.036        | NA                             | NA           | NA           | NA        | NA          | NA          | NA          | NA          | NA          | NA        |
|   | Average   | <b>622</b>                           | <b>3772</b> | <b>14334</b> | <b>70</b>  | <b>58239</b>  | <b>0.099</b>                        | <b>0.036</b> | <b>NA</b>                      | <b>NA</b>    | <b>NA</b>    | <b>NA</b> | <b>NA</b>   | <b>NA</b>   | <b>NA</b>   | <b>NA</b>   | <b>NA</b>   | <b>NA</b> |
| Unfumed Slag (post-1982 upper lift) <sup>b</sup>      | Minimum   | 77                                   | 1900        | <10          | 29         | 11119         | 0.009                               | 0.059        | 0.353                          | 0.043        | 0.021        | NA        | 0.023       | 1950        | 2200        | 1200        | 9.48        |           |
|   | Maximum   | 1840                                 | 23100       | 20300        | 325        | 149000        | 0.130                               | 0.4          | 0.62                           | 0.13         | 0.098        | NA        | 0.10        | 2650        | 3890        | 11750       | 9.97        |           |
|   | Average   | <b>755</b>                           | <b>7261</b> | <b>8453</b>  | <b>132</b> | <b>101874</b> | <b>0.072</b>                        | <b>0.196</b> | <b>0.529</b>                   | <b>0.097</b> | <b>0.066</b> | <b>NA</b> | <b>0.05</b> | <b>2173</b> | <b>3198</b> | <b>7225</b> | <b>9.66</b> |           |
| Fumed Slag <sup>c</sup>                               | Minimum   | 17                                   | 701         | <10          | <5         | 2080          | 0.028                               | NA           | 0.028                          | 0.056        | 0.02         | NA        | 0.788       | 54          | 45          | 480         | 6.16        |           |
|   | Maximum   | 377                                  | 5030        | 4425         | 14         | 28800         | 0.028                               | NA           | 0.054                          | 0.28         | 0.045        | NA        | 3.7         | 74          | 85          | 1450        | 7.77        |           |
|   | Average   | <b>90</b>                            | <b>1584</b> | <b>136</b>   | <b>10</b>  | <b>11718</b>  | <b>0.028</b>                        | <b>NA</b>    | <b>0.037</b>                   | <b>0.153</b> | <b>0.028</b> | <b>NA</b> | <b>2.65</b> | <b>65</b>   | <b>70</b>   | <b>1179</b> | <b>7.34</b> |           |

Notes:

NA = not analyzed

<sup>a</sup>Older unfumed slag totals from DH-69, -69, -76. SPLP results from DH-76 (one sample).

<sup>b</sup>Younger (upper lift) unfumed slag totals from DH-55, -74, -75, -76. SPLP results from DH-74 and DH-76 (three samples).

<sup>c</sup>Fumed slag totals from DH-55, -56, -65, -74, -75. SPLP results from DH-55 (one sample).

mg/kg = milligrams per kilogram

mg/L = milligrams per liter

RFI = RCRA Facility Investigation

RI/FS = Remedial Investigation/Feasibility Study

SPLP = synthetic precipitation leaching procedure

**Table 3-7. Constituent of Potential Concern Concentrations in Soil**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Sample   | As   | Pb   | Sb  | Ba   | Cd   | Cr   | Co  | Cu   | Fe    | Mn   | Se    | Ag   | Tl   | V    | Zn   | Hg    | Cr VI |
|--|------|------|-----|------|------|------|-----|------|-------|------|-------|------|------|------|------|-------|-------|
| <b>Surface Soil</b>                            |      |      |     |      |      |      |     |      |       |      |       |      |      |      |      |       |       |
| <b>Parcel 2a - Sampled 1991-2008</b>           |      |      |     |      |      |      |     |      |       |      |       |      |      |      |      |       |       |
| ASP-1  | 64   | 547  | -   | -    | 14   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| ASP-2  | 59   | 661  | -   | -    | 19   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| ASP-3  | 81   | 1190 | -   | -    | 18   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| ASP-4  | 172  | 1941 | -   | -    | 37   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| ASP-5  | 158  | 1444 | -   | -    | 30   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| EH-66  | 19.7 | -    | < 5 | 134  | 3.2  | 11.9 | < 5 | 24.3 | 12500 | 224  | 58.9  | 5.6  | 20.9 | 37.4 | 65.2 | < 0.5 | -     |
| EH-67  | < 5  | 23.5 | < 5 | 53.2 | < 1  | 9.2  | < 5 | 17.8 | 15100 | 222  | < 5   | < 5  | < 5  | 36.9 | 31   | < 0.5 | -     |
| EH-121   | 26.7 | -    | < 5 | 162  | 3.2  | 12.3 | < 5 | 21.7 | 12400 | 274  | 57.3  | < 5  | 20.9 | 43   | 70.6 | < 0.5 | -     |
| S25-J4   | 108  | 2920 | -   | -    | 63   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-J5   | 51   | 587  | -   | -    | 16   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-J6   | 39   | 221  | -   | -    | 8    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-K4   | 87   | 541  | -   | -    | 11   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-K5   | 93   | 1104 | -   | -    | 23   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-K6   | 73   | 806  | -   | -    | 15   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-L6-1                                       | 330  | 1492 | -   | -    | 43   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| S25-L6-2                                       | 231  | 2300 | -   | -    | 35   | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| <b>Parcel 2a - Sampled April 17 - 24, 2016</b> |      |      |     |      |      |      |     |      |       |      |       |      |      |      |      |       |       |
| P2a-DU1  | 246  | 2390 | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU2  | 223  | 2110 | 6   | 152  | 28.9 | 21   | 10  | 318  | 24600 | 3080 | 0.6   | 19.4 | 0.8  | 54   | 2280 | 1.8   | < 0.3 |
| P2a-DU3 <sup>a</sup>                           | 92   | 637  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU4  | 69   | 631  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU5  | 86   | 635  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU6  | 136  | 1480 | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU7  | 108  | 884  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU8  | 40   | 420  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU9  | 69   | 666  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU10 <sup>b</sup>                          | 92   | 794  | 2.7 | 147  | 13.8 | 22.4 | 10  | 192  | 23700 | 1460 | 0.9   | 6.1  | 0.8  | 54   | 1080 | 1.4   | < 1   |
| P2a-DU11                                       | 67   | 566  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU12                                       | 103  | 1110 | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU13                                       | 111  | 1120 | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU14                                       | 34   | 543  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU15                                       | 27   | 350  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU16                                       | 99   | 893  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU17 <sup>b</sup>                          | 69   | 541  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU18                                       | 114  | 1030 | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU19                                       | 28   | 259  | 1.5 | 137  | 7.3  | 21.1 | 7   | 64   | 21300 | 469  | < 0.5 | 1.4  | 0.6  | 51   | 153  | 0.64  | < 1   |
| P2a-DU20                                       | 27   | 388  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU21                                       | 39   | 423  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |
| P2a-DU22                                       | 95   | 800  | -   | -    | -    | -    | -   | -    | -     | -    | -     | -    | -    | -    | -    | -     | -     |

**Table 3-7. Constituent of Potential Concern Concentrations in Soil**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Sample                                     | As  | Pb   | Sb   | Ba  | Cd   | Cr   | Co  | Cu  | Fe    | Mn   | Se   | Ag  | Tl  | V  | Zn     | Hg   | Cr VI |
|--|-----|------|------|-----|------|------|-----|-----|-------|------|------|-----|-----|----|--------|------|-------|
| P2a-DU23                                   | 130 | 1060 | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P2a-DU28                                   | 99  | 729  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P2a-DU24                                   | 21  | 142  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P2a-DU25                                   | 27  | 316  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P2a-DU26                                   | 36  | 534  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P2a-DU27                                   | 106 | 902  | 3.1  | 126 | 17.3 | 18.3 | 9   | 179 | 19700 | 1690 | 0.6  | 7.1 | 0.9 | 45 | 1050   | 1.3  | < 1   |
| <b>Parcel 15 - sampled 1984-2001</b>       |     |      |      |     |      |      |     |     |       |      |      |     |     |    |        |      |       |
| 41   | 110 | 620  | 0.45 | 168 | 18   | 14   | 8.5 | 60  | 14100 | 321  | 0.07 | 1.9 | 0.5 | 32 | 177.91 | 2.9  | -     |
| 43   | 46  | 373  | 0.27 | 153 | 12   | 11   | 8   | 38  | 13500 | 474  | 0.55 | 0.8 | 0.6 | 22 | 114.91 | 2.1  | -     |
| S1AP-1                                     | 95  | 1911 | -    | -   | 37   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-10                                    | 122 | 2726 | -    | -   | 48   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-11                                    | 126 | 2758 | -    | -   | 51   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-12                                    | 188 | 5162 | -    | -   | 85   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-13                                    | 161 | 4263 | -    | -   | 70   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-14                                    | 148 | 4026 | -    | -   | 92   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-15                                    | 144 | 3313 | -    | -   | 88   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-16                                    | 63  | 1469 | -    | -   | 36   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-17                                    | 81  | 1538 | -    | -   | 42   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-18                                    | 32  | 45   | -    | -   | < 5  | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-2                                     | 69  | 1022 | -    | -   | 33   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-3                                     | 67  | 1070 | -    | -   | 28   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-4                                     | 77  | 1113 | -    | -   | 24   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-5                                     | 85  | 1272 | -    | -   | 38   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-6                                     | 74  | 1143 | -    | -   | 32   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-7                                     | 102 | 1736 | -    | -   | 44   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-8                                     | 104 | 2398 | -    | -   | 38   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| S1AP-9                                     | 107 | 2448 | -    | -   | 50   | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| <b>Parcel 15 - sampled May 5 - 8, 2016</b> |     |      |      |     |      |      |     |     |       |      |      |     |     |    |        |      |       |
| P15-DU1                                    | 75  | 480  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU2                                    | 35  | 367  | 1.8  | 174 | 10.7 | 22.7 | 7   | 76  | 18900 | 526  | 0.9  | 1.9 | 0.9 | 46 | 315    | 0.82 | < 1   |
| P15-DU3                                    | 54  | 2020 | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU4                                    | 49  | 369  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU5                                    | 55  | 453  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU6                                    | 61  | 865  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU7                                    | 44  | 410  | 1.5  | 198 | 13   | 25.2 | 8   | 58  | 19700 | 437  | 0.9  | 1.9 | 0.9 | 55 | 165    | 1.6  | < 1   |
| P15-DU8                                    | 50  | 746  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU9                                    | 37  | 402  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU10 <sup>3</sup>                      | 35  | 378  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU11                                   | 34  | 284  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU12 <sup>3</sup>                      | 35  | 314  | 1.2  | 175 | 9.7  | 26.8 | 9   | 46  | 21800 | 467  | 0.9  | 1.5 | 0.9 | 58 | 128    | 1.1  | < 1   |
| P15-DU13                                   | 34  | 237  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |
| P15-DU14                                   | 34  | 238  | -    | -   | -    | -    | -   | -   | -     | -    | -    | -   | -   | -  | -      | -    | -     |

**Table 3-7. Constituent of Potential Concern Concentrations in Soil**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Sample                                      | As   | Pb   | Sb   | Ba  | Cd   | Cr   | Co | Cu  | Fe    | Mn   | Se    | Ag  | Tl   | V  | Zn     | Hg   | Cr VI |
|---|------|------|------|-----|------|------|----|-----|-------|------|-------|-----|------|----|--------|------|-------|
| P15-DU15                                    | 29   | 275  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P15-DUA1                                    | 65   | 971  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P15-DUA2                                    | 49   | 706  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P15-DUA3                                    | 109  | 1890 | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P15-DUA4                                    | 66   | 741  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P15-DUA5 <sup>a</sup>                       | 26   | 489  | 1.6  | 116 | 11.5 | 15.9 | 8  | 103 | 19700 | 356  | 0.8   | 3   | 0.8  | 58 | 236    | 1.2  | < 1   |
| <b>Parcel 23 - Sampled 1984-2001</b>        |      |      |      |     |      |      |    |     |       |      |       |     |      |    |        |      |       |
| 69  | 65   | 417  | 0.27 | 163 | 14   | 12   | 9  | 43  | 12500 | 430  | 0.07  | 1.4 | 0.46 | 17 | 127.91 | 2.5  | -     |
| S12AP01-4                                   | 57   | 422  | -    | -   | 7    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| S12AP01-5                                   | 78   | 739  | -    | -   | 17   | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| <b>Parcel 23 - Sampled April 6-17, 2016</b> |      |      |      |     |      |      |    |     |       |      |       |     |      |    |        |      |       |
| P23-DU1                                     | 68   | 510  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU2                                     | 63.7 | 456  | 1.9  | 131 | 12.4 | 23.6 | 9  | 100 | 22800 | 749  | 1.6   | 3.4 | 0.9  | 57 | 448    | 1.4  | < 0.3 |
| P23-DU3 <sup>a</sup>                        | 78   | 524  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU4                                     | 87   | 621  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU5                                     | 78   | 505  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU6                                     | 42   | 479  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU7                                     | 70   | 519  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU8                                     | 65   | 409  | 1.5  | 138 | 10.1 | 25.6 | 10 | 91  | 23400 | 790  | 1.3   | 3.3 | 0.8  | 62 | 434    | 1.4  | < 1   |
| P23-DU9                                     | 58   | 340  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU10                                    | 64   | 420  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU11                                    | 62   | 363  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU12                                    | 49   | 266  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU13                                    | 52   | 403  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU14                                    | 39   | 221  | 0.9  | 117 | 4.5  | 20.4 | 9  | 58  | 20800 | 1120 | < 0.5 | 1.6 | 0.4  | 58 | 400    | 0.6  | < 1   |
| P23-DU15                                    | 53   | 438  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU16                                    | 53   | 297  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU17 <sup>a</sup>                       | 52   | 376  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU18                                    | 66   | 399  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU19                                    | 64   | 429  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU20 <sup>a</sup>                       | 57   | 357  | 1.6  | 155 | 10.4 | 24.5 | 11 | 90  | 24500 | 824  | 0.9   | 2.6 | 0.9  | 58 | 497    | 1.6  | < 1   |
| P23-DU21                                    | 79   | 476  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU22                                    | 72   | 400  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU23                                    | 36   | 214  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU24                                    | 60   | 336  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU25                                    | 55   | 297  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU26                                    | 44.6 | 331  | 1    | 115 | 10.8 | 22   | 9  | 90  | 23600 | 500  | 0.9   | 1.8 | 0.8  | 68 | 510    | 1.6  | < 0.3 |
| P23-DU27                                    | 39   | 262  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU28 <sup>a</sup>                       | 29.2 | 198  | 0.8  | 76  | 3.8  | 23   | 6  | 52  | 20000 | 673  | < 0.5 | 1.4 | 0.3  | 56 | 427    | 0.19 | 0.98  |
| P23-DU29                                    | 40   | 260  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |
| P23-DU30                                    | 59   | 377  | -    | -   | -    | -    | -  | -   | -     | -    | -     | -   | -    | -  | -      | -    | -     |

**Table 3-7. Constituent of Potential Concern Concentrations in Soil**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Sample Location                 | As   | Pb   | Sb | Ba | Cd  | Cr | Co | Cu   | Fe | Mn | Se   | Ag | Ti | V | Zn   | Hg | Cr VI |
|---------------------------------|------|------|----|----|-----|----|----|------|----|----|------|----|----|---|------|----|-------|
| <b>Subsurface Soil</b>          |      |      |    |    |     |    |    |      |    |    |      |    |    |   |      |    |       |
| <b>Parcel 2a - Sampled 2008</b> |      |      |    |    |     |    |    |      |    |    |      |    |    |   |      |    |       |
| EH-121-02                       | 27.8 | -    | -  | -  | 3.4 | -  | -  | 18   | -  | -  | 46.5 | -  | -  | - | 39.3 | -  | -     |
| EH-121-03                       | 31.8 | -    | -  | -  | 3.9 | -  | -  | 29   | -  | -  | 29   | -  | -  | - | 37.8 | -  | -     |
| EH-66-02                        | 19.7 | -    | -  | -  | 2.9 | -  | -  | 13.7 | -  | -  | 49.7 | -  | -  | - | 35.9 | -  | -     |
| EH-66-03                        | 28.8 | -    | -  | -  | 2.8 | -  | -  | 23.1 | -  | -  | 18.8 | -  | -  | - | 34.4 | -  | -     |
| EH-67-02                        | 5.2  | 50.5 | -  | -  | 4.6 | -  | -  | 29.3 | -  | -  | 28.9 | -  | -  | - | 54.7 | -  | -     |
| EH-67-03                        | < 5  | 141  | -  | -  | 7.3 | -  | -  | 46.6 | -  | -  | 36.4 | -  | -  | - | 89.4 | -  | -     |

Notes:

Results presented in milligrams per kilogram.

Ag = silver; As = arsenic; Ba = barium; Ca = calcium; Cd = cadmium; Co = cobalt; Cr = chromium; Cr VI = hexavalent chromium; Cu = copper; Fe = iron; Hg = mercury; Mn = manganese; Pb = lead; Sb = antimony; Se = selenium; Ti = titanium; V = vanadium ; Zn = zinc.

<sup>a</sup>The highest value is shown at field duplicate sample locations.

Subsurface soil sample interval reflected in sample location ID as follows:

02 = 2 to 4 feet below ground surface (bgs)

03 = 4 to 6 feet bgs



**Table 3-8. Constituent of Potential Concern Concentrations in Sediment**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| <b>Sample Identification</b> | <b>Sample Location</b> | <b>As (mg/kg)</b> | <b>Pb (mg/kg)</b> |
|------------------------------|------------------------|-------------------|-------------------|
| 23-1-SD                      | Upstream               | 25                | 150               |
| 23-2-SD                      | Upstream               | 15                | 83                |
| 23-3-SD <sup>a</sup>         | Upstream               | 20                | 95                |
| 23-4-SD                      | Upstream               | 19                | 152               |
| 23-5-SD                      | Upstream               | 10                | 47                |
| 2a-1-SD                      | Downstream             | 12                | 83                |
| 2a-2-SD                      | Downstream             | 54                | 402               |
| 2a-3-SD                      | Downstream             | 21                | 132               |
| 2a-4-SD <sup>a</sup>         | Downstream             | 33                | 284               |
| 2a-5-SD                      | Downstream             | 18                | 85                |
| 2a-6-SD                      | Downstream             | 20                | 139               |
| 2a-7-SD                      | Downstream             | 46                | 306               |
| 2a-8-SD                      | Downstream             | 20                | 106               |
| 2a-9-SD                      | Downstream             | 33                | 188               |
| 2a-10-SD                     | Downstream             | 26                | 138               |
| 2a-11-SD                     | Downstream             | 32                | 201               |

<sup>a</sup>The highest value is shown at field duplicate sample locations.

Notes:

mg/kg = milligrams per kilogram

As = arsenic

Pb = lead

**Table 3-9. Hydraulic Parameters by Source Area**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Source Area   | Average Saturated Thickness (ft) | Conductivity (ft/day) [K <sub>a</sub> ] | 2014 Gradient [i] (ft/ft) | Effective Porosity [n <sub>e</sub> ] (%) | Seepage Velocity (ft/day) |
|---------------|----------------------------------|---|---------------------------|--|---------------------------|
| West Selenium | 4                                | 200                                     | 0.0087                    | 18                                       | 9.7                       |
| North Plant   | 10                               | 200                                     | 0.0085                    | 18                                       | 9.4                       |
| Speiss-Dross  | 36                               | 140                                     | 0.011                     | 18                                       | 8.6                       |
| Acid Plant    | 11                               | 50                                      | 0.0193                    | 12                                       | 8.0                       |

Seepage Velocity Calculated via:

$$v = \frac{K_a i}{n_e}$$

where:

v= seepage velocity (ft/day)

K<sub>a</sub> = hydraulic conductivity (ft/day)

i = gradient

n<sub>e</sub> = effective porosity

Table 4-1. Summary of Human Health Risk Assessment Exposure Point Concentrations in Soil and Sediment

Corrective Measures Study Report, Former ASARCO East Helena Facility

| Parcel                            | Medium   | Depth Grouping        | Exposure Scenario     | Analyte   | EPC (mg/kg) | Commercial/Industrial MCS | Recreational MCS | EPC Exceeds MCS?                          | Notes     | Arsenic Risk |
|-----------------------------------|----------|-----------------------|-----------------------|---|-------------|---------------------------|------------------|---|-----------|--------------|
| 2a                                | Sediment | Surface               | Recreational          | Arsenic   | 45.47       | na                        | 794              | no  | EPC < MCS | 8.6E-06      |
|                                   |          |                       |                       | Lead  | 306.2       |                           | 3245             | no  | EPC < MCS |              |
|                                   | Soil     | Surface               | Commercial/Industrial | Arsenic   | 133.5       | 573                       | na               | no  | EPC < MCS |              |
|                                   |          |                       |                       | Lead  | 1169        | 800                       | yes              | <b>EPC &gt; Commercial/Industrial MCS</b> |           |              |
| 15                                | Soil     | Subsurface            | Commercial/Industrial | Arsenic   | 29.8        | 573                       | na               | no  | EPC < MCS | 1.7E-05      |
|                                   |          |                       |                       | Lead  | 64.07       | 800                       | no               | EPC < MCS                                 |           |              |
| 23                                | Sediment | Surface               | Recreational          | Arsenic   | 29.91       | na                        | 794              | no  | EPC < MCS | 5.6E-06      |
|                                   |          |                       |                       | Lead  | 204         |                           | 3245             | no  | EPC < MCS |              |
|                                   | Soil     | Surface               | Commercial/Industrial | Arsenic   | 69.31       | 573                       | na               | no  | EPC < MCS |              |
|                                   |          |                       |                       | Lead  | 465.2       | 800                       | no               | EPC < MCS                                 |           |              |
| Parcels 8W, 10, 11, 12, 17 and 18 | Soil     | Surface               | Commercial/Industrial | These parcels were remediated as part of the SPHC IM and do not exceed a EPC compared to MCS; significant excavation was needed to relocate PPC and excavated areas outside the new creek channel were backfilled using soil with concentrations below the MCSs. Potential human exposures to concentrations in soil higher than MCSs are therefore not expected to occur at these parcels. |             |                           |                  |   |           |              |
| Subsurface                        |          | Commercial/Industrial |                       |   |             |                           |                  |   |           |              |

Notes:

mg/kg = milligrams per kilogram

EPC = Exposure Point Concentration. Note that the maximum Chebyshev-based UCL was selected as the EPC for ISM samples (ITRC, 2012) and the maximum recommended UCL was selected for discrete samples.

EPC values considered the potential exposure pathways for soil ingestion (direct contact) and inhalation of dust suspended into the air

MCS = Media Cleanup Standard

na = not applicable

ND = non-detect

UCL = 95 percent Upper Confidence Limit

Subsurface = greater than 2 feet below ground surface

Surface = 0 to 2 feet below ground surface

Arsenic risks are characterized by calculating lifetime cancer risks. See Appendix E for details of the calculation.

Lead risks are characterized by directly comparing the EPC with the MCS. The MCSs for lead are based on a blood-lead level of 10 µg/dL.

µg/dL = micrograms per deciliter

**Table 4-2. Summary of Ecological Risk Assessment Exposure Point Concentrations in Soil**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Parcel                     | Medium | Depth Grouping | Analyte | EPC (mg/kg) | MCS (mg/kg) | Receptor for MCS | HQ  | Explanatory Notes   |
|----------------------------|--------|----------------|---------|-------------|-------------|------------------|-----|---|
| 2a                         | Soil   | Surface        | Lead    | 1169        | 650         | Passerine birds  | 1.8 | Population-level effects are unlikely with an HQ slightly elevated above one  |
|                            |        |                |         | 1169        | 955         | Cattle           | 1.2 |   |
| 15                         | Soil   | Surface        | Lead    | 1028        | 650         | Passerine birds  | 1.6 |   |
|                            |        |                |         | 1028        | 955         | Cattle           | 1.1 |   |
| 23                         | Soil   | Surface        | Lead    | 465.2       | 650         | Passerine birds  | 0.7 | HQ < 1  |
|                            |        |                |         | 465.2       | 955         | Cattle           | 0.5 |   |
| 8W, 10, 11, 12, 17, and 18 | Soil   | Surface        |         |             |             |                  |     | These parcels were remediated as part of the South Plant Hydraulic Control interim measure and do not exceed an EPC compared to MCS; significant excavation was needed to relocate Prickly Pear Creek and excavated areas outside the new creek channel were backfilled using soil with concentrations below the MCSs. Potential human exposures to concentrations in soil higher than MCSs are therefore not expected to occur at these parcels. |

**Notes:**

mg/kg = milligrams per kilogram

EPC = exposure point concentration. Note that the maximum Chebyshev-based upper confidence limit (UCL) was selected as the EPC for ISM samples (ITRC, 2012) and the maximum recommended UCL was selected for discrete samples.

HQ = hazard quotient

MCS = media cleanup standard

**Table 4-3. Remaining Unacceptable Risk Post-Interim Measure Construction**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| CMS Parcel             | Exposure Media                    | Receptors                                 | Potential Exposure | Assessment of Potential                           |   |
|------------------------|-----------------------------------|---|--------------------|---|---|
|                        |                                   |   | Pathway            | Exposure  | Assessment of Risks   |
| 2a                     | Soil                              | Industrial/<br>Commercial<br>Recreational | Direct contact     | Pathways potentially complete                     | Overall lead exposures are lower than levels protective of human health (i.e., blood-lead levels are less than 10 µg/dL). Concentrations of arsenic fall within target risk range.        |
|                        |                                   | Ecological (passarine)                    | Direct contact     | Pathway potentially complete                      |   |
|                        | Sediment                          | Recreational                              | Direct Contact     | Pathways potentially complete                     | Overall lead exposures are lower than levels protective of human health (i.e., blood-lead levels less than 10 µg/dL). Concentrations of arsenic fall within target risk range.            |
|                        | Groundwater                       | Residential                               | Ingestion          | Potentially complete <sup>a</sup>                 | None: concentration of arsenic and selenium are below MCS (i.e., drinking water MCLs).  |
| 8W, 10, 11, 12, 17, 18 | Soil<br>Sediment<br>Surface water | Recreational                              | Direct contact     | Potentially complete                              | Risk unlikely to be present due to implementation of SPHC IM to meet MCSs.  |
| 15                     | Soil                              | Industrial/<br>Commercial                 | Direct contact     | Pathway complete under current or future land use | Lead concentrations fall below MCS and levels protective of human health; lifetime cancer risk from arsenic falls within target risk range.   |
|                        |                                   | Ecological (passarine)                    | Direct contact     | Pathway potentially complete                      | Risk from concentrations of lead are minimal and do not require remediation.  |
|                        | Groundwater                       | Residential                               | Ingestion          | Potentially complete <sup>a</sup>                 | Concentration of arsenic (West Arsenic Source Area) higher than MCS (i.e., drinking water MCLs).  |
| 16, 19                 | Soil                              | Ecological (passarine)                    | Direct contact     | Potentially complete                              | Risk unlikely to be present due to implementation of ET Cover System IM to meet MCSs.   |
|                        | Groundwater                       | None                                      | None               | Incomplete  | None: groundwater use is prohibited within the Facility.  |
|                        | Unfumed Slag                      | Trespasser                                | Direct contact     | Potentially complete                              | Risk not quantified due to ongoing evaluation of corrective measures.   |
| 23                     | Soil                              | Recreational                              | Direct contact     | Pathways potentially complete                     | Concentrations of lead and arsenic are lower than MCSs; overall lead exposures are lower than levels protective of human health; concentrations of arsenic fall within target risk range. |
|                        |                                   | Ecological (passarine)                    | Direct contact     | Pathway potentially complete                      |   |
|                        | Sediment                          | Recreational                              | Direct contact     | Pathways potentially complete                     | Concentrations of lead and arsenic are lower than MCSs; overall lead exposures are lower than levels protective of human health; concentrations of arsenic fall within target risk range. |

Note:

<sup>a</sup> Groundwater pathway potentially complete if used as a drinking water source.

MCS = media cleanup standard (see Table 2-1)

µg/dL = microgram(s) per deciliter

**Table 5-1. Overview of Source Area Screening-Level Evaluation**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

|                                 |  | <b>Remedy Screening Evaluation</b>   |   |
|---------------------------------|--|--|---|
| <b>Source Area<sup>a</sup></b>  | <b>Preliminary Alternative</b>   | <b>Notes on Scoring</b>  | <b>Recommended for Further Evaluation (Y/N)</b> |
| Affected Groundwater Area       | Baseline action: includes planned IMs, CGWA, and MNA                           | Baseline action will be implemented regardless of recommendation of the evaluation. All other potential groundwater remedies and their associated costs are considered supplemental. | NA  |
|                                 | Pump and treat onsite and offsite groundwater                                  | Not cost-effective.  | No  |
|                                 | Pump and treat onsite groundwater  | Not cost-effective.  | No  |
|                                 | Pump and treat combined with slurry wall                                       | Uncertain effects on downgradient plume stability and geometry and not cost effective.   | No  |
| West Selenium Source Area       | Source Removal   | Recommend using the groundwater flow model to determine effectiveness in comparison to other remedies. Moderate cost.  | Yes   |
|                                 | PRB, with funnel-and-gate system   | Favorable effectiveness and implementability with low cost.  | Yes   |
|                                 | Slurry Wall (hydraulic enclosure of source area)                               | Slurry walls have been shown to be effective and appears to be cost-effective.   | Yes   |
|                                 | Focused pump and treat   | Reasonably effective, and favorable implementability with potential for low cost.  | Yes   |
| North Plant Arsenic Source Area | Source Removal   | Not cost-effective.  | No  |
|                                 | PRB, with funnel-and-gate system   | Effective, technology is readily available, reasonably cost-effective.   | Yes   |
|                                 | Slurry Wall (hydraulic enclosure of source area)                               | Slurry walls have been observed to be effective and appears to be cost-effective.  | Yes   |
|                                 | In-situ treatment (dosing of aquifer with Fe), to augment slurry wall          | Can be effective if used in conjunction with slurry wall.  | Yes   |
|                                 | In-situ treatment (to augment slurry wall)                                     | High costs and difficult to implement.   | No  |
| Former Speiss/Dross Source Area | No Further Action (includes existing slurry walls)                             | Already implemented, and is cost-effective.  | NA  |
|                                 | Source Removal   | Additional cost not justified when existing slurry wall appears generally to be effective.   | No  |
|                                 | Expand slurry wall system to encompass former Speiss Storage and Handling Area | Technologies are available but high implementation factor due to technology being installed close to the Ore Storage Building.   | No  |
|                                 | In-situ treatment (dosing of aquifer with Fe), to augment slurry wall          | Would be effective with another technology such as a slurry wall, but not effective alone.   | No  |

<sup>a</sup> Further investigation and evaluation of the former Acid Plant and Slag Pile areas was deferred.

Notes:

CBS = combined balancing score

CGWA = Controlled Groundwater Area

Fe = ferrous sulfate

IM = interim measure

NA = not applicable

O&M = operations and maintenance

PRB = permeable reactive barrier

Se = selenium

Table 5-2. RCRA Balancing Criteria, Definitions, and Interpretation/Application to Remedy Evaluations  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| Balancing Criteria                          | Definition (per RCRA [USEPA, 2000])  | Interpretation and Application of Balancing Criteria to Remedy Evaluation   | Scoring Logic [ + positive, 0 neutral, - negative]  |
|---|--|---|---|
| 1. Long-term Effectiveness and Permanence   | Decision-makers should evaluate remedies based on the long-term reliability and effectiveness they afford, along with the degree of certainty that they will remain protective of human health and the environment. Additional considerations include the magnitude of risks that will remain at a site from untreated hazardous wastes, hazardous wastes and hazardous constituents, and treatment residuals; and the reliability of any containment systems and institutional controls. A remedial option should include a description of the approaches and facilities that will be used to assess long-term performance and effectiveness. | Criteria evaluated as the relative improvement in groundwater concentrations for the COPC of interest (selenium for West Selenium and arsenic in North Plant) as a result of implementing the alternative in addition to interim measures; and also the permanence the alternative provides. Model simulations (by Newfields) will be used to quantify effectiveness considering the following metrics: (1) mass removal (in weight and percent), (2) plume geometry/volume reductions below DEQ-7 water quality standards, and (3) the temporal timeframe to achieve stable ('steady-state') conditions following implementation. Alternatives providing the highest degree of long-term effectiveness are those that achieve the most mass and volume reductions, have the highest degree of permanence, leave little or no waste (source), do not require long-term maintenance, and minimize the need for institutional controls. | "+" = Highest degree or substantive improvements in groundwater metrics (reductions in mass and plume reduction); alternative is permanent over the long-term.<br>"0" = Moderate or marginal improvement in groundwater metrics; and/or some uncertainties or risks relative to permanence.<br>"-." = No substantive improvement in groundwater metrics and/or the alternative is lacking permanence or considered a high-risk, unproven technology.  |
| 2. Toxicity, Mobility, and Volume Reduction | Decision-makers should evaluate remedies based on the degree to which they employ treatment, including treatment of principal threats, that reduces the toxicity, mobility, or volume of hazardous wastes and hazardous constituents, considering, as appropriate: the treatment processes to be used and the amount of hazardous waste and hazardous constituents that will be treated; the degree to which treatment is irreversible; and the types of treatment residuals that will be produced.  | Criteria focus on the degree to which an alternative does or does not employ a treatment technology. For alternatives that require treatment technology (such as PRB, pump and treat, and injections), the evaluation will describe (1) quantities and quality (i.e., concentrations) of groundwater requiring treatment, (2) degree in which treatment is irreversible, and (3) types and volumes of treatment residuals. For alternatives that do not require a geochemical alteration/treatment technology (such as source removal and slurry wall), the volume of source material will be estimated.  | "+" = Alternative reduces toxicity and mobility of hazardous material; irreversible with limited or no residuals management.<br>"0" = Alternative reduces toxicity, mobility, or volume; irreversible but with some residuals for management.<br>"-." = Alternative has limited effect on toxicity, mobility, or volume reduction; reversible or has significant residual management.   |
| 3. Short-term Effectiveness                 | Decision-makers should evaluate remedies based on the short-term effectiveness and short-term risks that remedies pose, along with the amount of time it will take for remedy design, construction, and implementation.  | Criteria address the effects during construction and implementation (i.e., short-term) and will focus on (1) short-term impacts/risks to human health (related to construction), (2) short-term impacts (i.e., releases) to the environment related to implementation of remedy, and (3) and how long it will take to design, construct, and implement the alternative.   | "+" = No substantive risks/impacts to human health or environment. Short duration to establish effectiveness.<br>"0" = Moderate risks/impacts to human health or environment. Longer duration to establish effectiveness.<br>"-." = High-degree of risks/impact to human health or environmental impacts. Requires significant duration to establish effectiveness.   |
| 4. Implementability                         | Decision-makers should evaluate remedies based on the ease or difficulty of remedy implementation, considering as appropriate: the technical feasibility of constructing, operating, and monitoring the remedy; the administrative feasibility of coordinating with and obtaining necessary approvals and permits from other agencies; and the availability of services and materials, including capacity and location of needed treatment, storage, and disposal services.  | Criteria focus on (1) administrative components, (2) regulatory coordination and approvals, and (3) overall ease or difficulty of constructing, operating, and monitoring the remedy; including availability of services relative of the types of alternatives and/or complexity of specialty services needed. Alternatives that are considered easiest or most favorable to implement are those which (1) do not require substantive agency approval or permits, (2) do not require long-term O&M, and (3) do not rely on specialty technologies, services, or materials.  | "+" = Administrative items, regulatory approvals, construction, operation, and monitoring are considered relatively easy, feasible, or readily implementable. No long-term O&M. Short duration to implement alternative.<br>"0" = Neutral score if not easy or "complex." Longer duration to establish effectiveness.<br>"-." = Alternative requires agency substantive or nonstandard approvals or permits, substantive long-term O&M, specialty technology, and/or significant duration to implement alternative. |
| 5. Cost                                     | Decision-makers should evaluate remedies based on capital and O&M costs, and the net present value of the capital and O&M costs.   | Estimated costs have been developed for each alternative using Study or Feasibility Class 4 guidance (Association for the Advancement of Cost Engineering, 2005) with expected accuracy of -30 to +50 percent. Costs reflect both capital and long-term O&M (when applicable) assuming a 30-year period net present worth at 5 percent rate of return (unless specified otherwise). The total cost reflects capital and long-term O&M (if applicable). Costs are based on conceptual designs and are not considered final designs; if an alternative is selected, a final design will be developed before implementation.   | "+" = Relatively low. Cost is less than \$2M.<br>"0" = Moderate. Cost ranges from \$2 to \$5M.<br>"-." = Relatively high. Cost is greater than \$5M.  |
| 6. Community Acceptance                     | Decision-makers should evaluate remedies based on the degree to which they are acceptable to the interested community.   | The evaluation is based on the first five technical criteria (listed above). Community acceptance will be evaluated as part of the public involvement process.  |   |
| 7. State Acceptance                         | Decision-makers should evaluate remedies based on the degree to which they are acceptable to the state in which the subject facility is located. This is particularly important where the U.S. Environmental Protection Agency, not the state, selects the remedy.   | The evaluation is based on the first five technical criteria (listed above). State acceptance will be evaluated as part of the public involvement process.  |   |

- Notes:
- COC = constituent of concern
  - COPC = constituent of potential concern
  - M = million
  - MCL = maximum contaminant level
  - O&M = operations and maintenance
  - RCRA = Resource Conservation and Recovery Act

Reference: U.S. Environmental Protection Agency (USEPA). 2009. *Fact Sheet #3: Final Remedy Selection for Results-based RCRA Corrective Action*. RCRA Corrective Action Workshop on Results-Based Project Management: Fact Sheet Series. March.

Table 5-3. Description of Remedial Alternatives Retained for Detailed Evaluation  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| Area                                  | Alternative               | Technology Description/Assumptions  | Dimensions/Unit Quantities   | Construction Approach and Key Assumptions  |
|---------------------------------------|---------------------------|---|--|--|
| West Selenium Area (COPC is selenium) | 1 – Source Removal        | Assumes physical excavation and relocation of saturated zone source materials to an onsite location that is beneath the future ET cover but above the saturated zone. The alternative is expected to reduce ongoing mobilization and leaching of selenium from the primary source area to groundwater. Primary source area boundaries assumed to capture an estimated 70 percent of source/mass (personal communication with Bob Anderson/Hydrometrics, January 9, 2015). | Area 100 x 200 x 48 ft bgs. Quantity estimates: <ul style="list-style-type: none"> <li>Interim measure cover: 2,222 yd<sup>3</sup></li> <li>Unsaturated zone: 29,629 yd<sup>3</sup></li> <li>Saturated zone (source removal): 4,444 yd<sup>3</sup></li> <li>Backfill of clean borrow material: 4,444 yd<sup>3</sup> (West Bench)</li> </ul>  | <ul style="list-style-type: none"> <li>Saturated zone material placed under ICS-2 (and ET cover).</li> <li>Clean borrow material via West Bench placed in saturated zone.</li> <li>Unsaturated zone soils placed back into excavation in unsaturated zone.</li> <li>Dewatering limited because of soldier pile-sheet pile walls; sump-pump used to dewater saturated zone, groundwater pumped to temporary tank and hauled to existing treatment plant.</li> <li>All earthwork done onsite; no offsite hauling or disposal.</li> </ul>   |
|                                       | 2 – PRB for Selenium      | Technology assumes passive groundwater flow through the reactive media to treat selenium. PRB media consist of 90 percent organic mulch and 10 percent limestone sand placed across saturated interval. Influent selenium concentrations assume 3.0 mg/L; treatment targets assume 0.05 mg/L (MDEQ-7 groundwater standard). Media will have finite life and will require monitoring to determine when media needs replacement.  | 100-ft-long PRB with 25-ft funnels (slurry walls) at either end. PRB installed across saturated interval, wall width of 12 ft (perpendicular to flow) designed to achieve residence time of 2 days. Funnel walls installed from ash/clay to ground surface and designed to have limited influence on groundwater flow patterns.  | <ul style="list-style-type: none"> <li>Passive treatment of selenium considered ‘pilot study’; long-term viability/effectiveness uncertain. Limited formal research/documentation on full-scale studies over long-term.</li> <li>Construction approach assumes long-arm excavator to install PRB and funnel ends.</li> <li>Long-term O&amp;M assumes full replacement of PRB media in years 10 and 20; actual replacement schedule determined from monitoring/effectiveness.</li> <li>Spent media disposed of offsite; volume estimated at 444 yd<sup>3</sup>.</li> </ul>  |
|                                       | 3 – Slurry Wall Enclosure | Technology assumes an effective, low-permeability enclosure “wall” located around the primary source area saturated zone; design assumptions are to reduce the mobility/flux from within the enclosure area. Design assumes slurry wall permeability of 1x10 <sup>-6</sup> cm/sec or lower.   | Perimeter of 1,100 linear feet based on enclosure dimensions of 100 x 450 ft in plan view. Depth of slurry wall assumes 48 ft bgs down to ash/clay layer. Typical construction approach assumes slurry wall installed from ash/clay layer to ground surface.   | <ul style="list-style-type: none"> <li>Construction approach assumes long-arm excavator to install slurry wall and use of excavated soil in soil-bentonite blend.</li> <li>Permeability options: soil-bentonite wall 1x10<sup>-7</sup> cm/sec or cement-bentonite wall 1x10<sup>-6</sup> cm/sec; difference in cost is about \$3/VSF. Costing approach is conservative and assumes soil-bentonite wall.</li> </ul>   |
|                                       | 4 – Pump and Treat (P&T)  | Technology assumes a long-term groundwater extraction system extending across a width of about 100 ft (approximate width of plume) and then conveyance of groundwater to passive treatment system, which includes: <ul style="list-style-type: none"> <li>Biochemical reactor beds consisting of organic mulch, limestone, and sand</li> <li>Aeration channel</li> <li>Oxidation/settling ponds</li> <li>Discharge to existing wetlands and Prickly Pear Creek</li> </ul> | Groundwater Extraction System: <ul style="list-style-type: none"> <li>Three wells – combined total flow of 30 gallons per minute</li> <li>Buried conveyance pipe: about 4,800 ft</li> </ul> Treatment System: <ul style="list-style-type: none"> <li>Dual biochemical reactor beds: total volume 12,400 yd<sup>3</sup></li> <li>Dual oxidation ponds: total volume 584 yd<sup>3</sup></li> <li>See process flow diagram in Appendix C for details</li> </ul> | <ul style="list-style-type: none"> <li>P&amp;T option will require regulatory approvals and discharge permit to set monitoring requirements and effluent/discharge limits</li> <li>Treatment system will require routine maintenance (weekly), monitoring, and intermittent replacement of spent media. Costing approach assumes biochemical reactor beds are replaced at years 10 and 20; actual replacement cycle depends on monitoring.</li> <li>Treatment system will require winterization design for year-round operation (such as buried conveyance line, buried biochemical reactor beds, heat-traced lines, and heated blower or mechanical agitator). These items will add capital costs and also replacement costs to replace media.</li> </ul> |

Notes:

Alternative 7 (in-situ injections) is assumed supplemental to Alternative 6 (injections within the slurry wall). If Alternative 6 is selected, then the need for Alternative 7 may be evaluated and decided on after the slurry wall is constructed and the effectiveness evaluated, among other criteria.

Abbreviations:

- bgs = below ground surface
- cm/sec = centimeter(s) per second
- COPC = constituent of potential concern
- ET = evapotranspiration
- ft = foot/feet
- ICS = Interim Cover System
- MDEQ = Montana Department of Environmental Quality
- mg/L = milligram(s) per liter
- P&T = pump and treat
- PRB = permeable reactive barrier
- VSF = vertical square foot
- yd<sup>3</sup> = cubic yard
- ZVI = zero-valent iron



Table 5-3. Description of Remedial Alternatives Retained for Detailed Evaluation  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| Area                             | Alternative   | Technology Description/Assumptions  | Dimensions/Unit Quantities  | Construction Approach and Key Assumptions  |
|----------------------------------|---|---|---|--|
| North Plant<br>(COPC is arsenic) | 5 – PRB for Arsenic   | Technology assumes passive groundwater flow through the reactive media to treat arsenic. PRB media consist of 100 percent pure ZVI (granular iron) placed across saturated interval. Influent arsenic concentrations assume 20 to 25 mg/L; treatment targets assume 0.01 mg/L (MDEQ-7 groundwater standard). Media will have finite life and will require monitoring to determine when media needs replacement. | 400-ft-long PRB with 125-ft funnels at either end; alignment is adjusted to stay on Custodial Trust-owned property. PRB is 8 ft thick to achieve residence time of 2+ days. Funnel walls installed from ash/clay to ground surface and designed to have limited influence on groundwater flow patterns. | <ul style="list-style-type: none"> <li>Construction approach assumes long-arm excavator to install PRB and funnel ends</li> <li>Long-term O&amp;M assumes full replacement of PRB media in year 10 and 20; actual replacement schedule determined from monitoring/effectiveness.</li> <li>Spent media disposed of offsite; volume assumed at 2,370 yd<sup>3</sup>.</li> <li>Unit cost of pure ZVI is \$1,020/ton; volume estimates assume the PRB will require approximately 5,000 tons, which is about 75 percent of the overall cost.</li> </ul> |
|                                  | 6 – Slurry Wall Enclosure   | Technology assumes an effective, low-permeability enclosure “wall” located around source area saturated zone; design assumptions are to reduce mobility/flux from within the enclosure area. Design assumes slurry wall permeability of 1x10 <sup>-6</sup> cm/sec or lower.   | Perimeter of 1,560 linear feet. Depth of wall to 51 ft bgs to ash/clay layer. Alignment of wall adjusted to stay within Custodial Trust-owned property.   | <ul style="list-style-type: none"> <li>Construction approach assumes long-arm excavator to install slurry wall and use of excavated soil in soil-bentonite blend.</li> <li>Permeability options: soil-bentonite wall 1x10<sup>-7</sup> cm/sec or cement-bentonite wall 1x10<sup>-6</sup>cm/sec; difference in cost is about \$3/VSF. Costing approach is conservative and assumes soil-bentonite wall.</li> </ul>  |
|                                  | 7 - In-Situ Injections (in conjunction with Alternative 6 slurry wall enclosure). | Technology assumes installation of injection wells within slurry walls to deliver (via injection) nanoslurry mixture within slurry wall enclosure. ZVI nanoparticles have relatively high-surface area to volume ratio and are demonstrated to be effective at binding arsenic in solution.   | Design assumes five injection wells placed within the slurry wall enclosure. Injections assume ZVI micro/nanoparticles placed (injected) via slurry form. Treatment assumes 2.4M gallons within the slurry walls.   | <ul style="list-style-type: none"> <li>Conceptual-design estimates of weight/volume of ZVI nanoparticles assume 2 tons; however, actual volume needed for treatment dependent on batch testing and effectiveness monitoring after the first of four proposed injections.</li> <li>Unit cost of ZVI nanoparticles in dry form (to be mixed into slurry) assumed at \$40 per pound.</li> <li>Costs assume that the 2 tons (total) applied over four separate injection events.</li> </ul>  |

Notes:

Alternative 7 (in-situ injections) is assumed supplemental to Alternative 6 (injections within the slurry wall). If Alternative 6 is selected, then the need for Alternative 7 may be evaluated and decided on after the slurry wall is constructed and the effectiveness evaluated, among other criteria.

Abbreviations:

- bgs = below ground surface
- cm/sec = centimeter(s) per second
- COPC = constituent of potential concern
- ET = evapotranspiration
- ft = foot/feet
- ICS = Interim Cover System
- MDEQ = Montana Department of Environmental Quality
- mg/L = milligram(s) per liter
- P&T = pump and treat
- PRB = permeable reactive barrier
- VSF = vertical square foot
- yd<sup>3</sup> = cubic yard
- ZVI = zero-valent iron

Table 5-4. Combined Balancing Criteria Evaluation  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| Area                                | Alternative                               | Long-Term Effectiveness and Permanence | Reduction in Toxicity, Mobility, or Volume through Treatment | Short-Term Effectiveness | Implementability | Cost (\$millions)<br>(total cost includes capital and long-term O&M [if applicable])                                      | Combined Balancing Criteria Score (CBS) | Comments |
|-------------------------------------|---|--|--|--------------------------|------------------|---|---|----------|
| West Selenium<br>(COPC is selenium) | 1 – Source Removal                        | +                                      | +  | 0                        | 0                | 0<br><b>Total Cost: \$2.8M</b><br>Capital: \$2.8M<br>Long-term O&M: none  | +2                                      |          |
|                                     | 2 – PRB for Selenium                      | 0                                      | 0  | +                        | 0                | 0<br><b>Total Cost: \$2.8M</b><br>Capital: \$1.5M<br>Long-term O&M: \$1.3M  | +1                                      |          |
|                                     | 3 – Slurry Wall Enclosure                 | +                                      | 0  | +                        | +                | +<br><b>Total Cost: \$1.7M</b><br>Capital: \$1.7M<br>Long-term O&M: none  | +4                                      |          |
|                                     | 4 – Pump and Treat                        | 0                                      | 0  | +                        | -                | 0<br><b>Total Cost: \$4.1M</b><br>Capital: \$2.4M<br>Long-term O&M: \$1.7   | 0                                       |          |
| North Plant<br>(COPC is arsenic)    | 5 – PRB for Arsenic                       | 0                                      | -  | +                        | 0                | -<br><b>Total Cost: \$20M</b><br>Capital: \$10M<br>Long-term O&M: \$10  | -1                                      |          |
|                                     | 6 – Slurry Wall Enclosure                 | 0                                      | -  | +                        | +                | 0<br><b>Total Cost: \$2.1M</b><br>Capital: \$2.1M<br>Long-term O&M: none  | +1                                      |          |
|                                     | 7 – Slurry Wall Enclosure with Injections | 0                                      | -  | +                        | +                | 0<br><b>Total Cost: \$2.5M</b><br>ALT6: \$2.1M<br>ALT7 Capital: \$0.1M (wells)<br>ALT7 Long-term O&M: \$0.3M (injections) | +1                                      |          |

Notes:

Cost assumptions: long-term O&M assumed 30 years with Net Present Worth at 5 percent rate of return; refer to *Tier II Source Control Measure/Groundwater Remedy Evaluation—Phase 2 Results and Recommendations* (CH2M, 2015), included in Appendix C of the CMS Report, for supporting ROM Class 4 costing information.

Refer to Table 5-3 for alternative descriptions, Table 5-4 for balancing criteria and definitions, and Appendix B for tables that show details on the individual balancing criteria evaluation.

Alternative 7 is slurry wall with injections. If Alternative 6 is selected, then the need for Alternative 7 may be decided after the slurry wall is constructed and the effectiveness is evaluated.

CBS = combined balancing score

COPC = constituent of potential concern

M = million

O&M = operations and maintenance

P&T = pump and treat

PRB = permeable reactive barrier

**Table 5-5. Overview of Source Area Remedy Evaluation Results**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

|                           |  | <b>Remedy Evaluation</b>   |  |
|---------------------------|--|--|--|
| <b>Source Area</b>        | <b>Carried Forward from Screening-level</b>      |  | <b>Evaluation Results</b>  |
|                           | <b>Evaluation</b>                                | <b>Notes on Scoring</b>  |  |
| West Selenium Source Area | Source Removal                                   | CBS of plus two (+2); would be more effective at reducing toxicity, mobility, or volume through treatment; with uncertainty of source capture and cost limiting the overall score.   | Recommend supplemental data and additional modeling to support continued evaluation. |
|                           | PRB, with funnel-and-gate system                 | CBS of plus one (+1); a positive score for short-term effectiveness, but with lack of proven Se removal effectiveness and cost requirements for O&M limit the overall score.   | Not evaluated further.   |
|                           | Slurry Wall (hydraulic enclosure of source area) | Highest CBS of plus four (+4); long-term effectiveness and permanence, short-term effectiveness, implementability, and cost.   | Recommend supplemental data and additional modeling to support continued evaluation. |
|                           | Focused pump and treat                           | Combined balancing score at neutral (0); negative scoring based on implementation with moderate cost effectiveness.  | Not evaluated further.   |
| North Plant Arsenic Area  | PRB, with funnel-and-gate system                 | CBS of negative one (-1); with positive score for short-term effectiveness, but negative scores on reduction in toxicity, mobility, or volume through treatment; the lack of significant contaminant mass and plume volume <u>reduction and the cost limit the score</u> . | Not evaluated further.   |
|                           | Slurry Wall (hydraulic enclosure of source area) | CBS of plus two (+2); positive scores for short-term effectiveness and implementability; the lack of significant contaminant mass and plume volume reduction and contaminated groundwater that remains within the slurry wall long-term limits the score.                  | Recommend supplemental data and additional modeling to support continued evaluation. |
|                           | Slurry Wall Enclosure with In-situ treatment     | CBS of plus three (+3); positive scores for reduction in toxicity, mobility, or volume through treatment, short-term effectiveness, and implementability. The <u>remaining criteria were scored 0 (neutral)</u> .  | To be considered based on evaluation results of previous alternative (Slurry Wall).  |

Notes:

CBS = combined balancing score

CGWA = Controlled Groundwater Area

Fe = ferrous sulfate

IM = interim measure

NA = not applicable

O&M = operations and maintenance

PRB = permeable reactive barrier

Se = selenium

**Table 5-6. Summary of Predictive Results from Groundwater Flow Model**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| <b>Model Scenario</b>                           | <b>Constituent</b> | <b>Mass Flux Rate Across Facility Boundary (grams/day)</b> | <b>Flux Rate Decrease from 2011 (percent)</b> |
|---|--------------------|--|---|
| Groundwater 2011                                | Arsenic            | 11,300   | 0%  |
| Groundwater 2011                                | Selenium           | 581  | 0%  |
| Groundwater 2014                                | Arsenic            | 6,054  | 47%   |
| Groundwater 2014                                | Selenium           | 360  | 38%   |
| Predicted IM 2025                               | Arsenic            | 3,874  | 66%   |
| Predicted IM 2025                               | Selenium           | 188  | 68%   |
| Predicted IM with Acid Plant (70%) Removal 2025 | Arsenic            | 3,862  | 66%   |
| Predicted IM WSA Finite Mass 2025               | Selenium           | 178  | 69%   |

Notes:

IM = Interim Measure

WSA = West Selenium Area

**Table 5-7. Estimated Selenium Reduction for Slag Pile Cover Alternatives**  
*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Cover Alternative                              | Estimated % Reduction of Selenium in Groundwater in General Areas |   |   |   |
|--|---|---|---|---|
|  | Slag Pile<br>(DH-10A, 56, and 74)                                 | Downgradient of Slag Pile<br>(DH-6, 15, and 51) | Lamping Field Area<br>(EH-126, 138, and<br>139) | Canyon Ferry Road<br>Area<br>(EH-142 and 143) |
| Minimum  | 73%   | 69%   | 35%   | 38%   |
| Intermediate                                   | 76%   | 73%   | 38%   | 41%   |
| Maximum  | 94%   | 93%   | 56%   | 58%   |
| <i>GW Model Estimate<br/>10% Recharge Rate</i> | <i>85%</i>  | <i>83%</i>                                      | <i>47%</i>                                      | <i>50%</i>                                    |

**Table 6-1. Summary of Proposed Corrective Measures and Supplemental Institutional Controls**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Proposed Remedy Elements  | Engineering/Activity Components   | Applicable Parcels   | Applicable Media or Pathway |
|---|---|--|-----------------------------|
| <b>ENGINEERING CONTROLS</b>   |   |  |                             |
| ET Cover System - Building Demolition, Utility Abandonment, Subgrade Fill, Final ET Cover                             | ET Cover to mitigate infiltration of precipitation, control wind erosion  | Facility (Parcels 16,19)                                   | Groundwater                 |
|   | Surface water/stormwater collection   |  | Soil                        |
| South Plant Hydraulic Controls: Upper Lake and Lower Lake Removal; PPC Bypass; PPC Realignment; wetland construction  | Reduce surface water loading to groundwater by removing Upper Lake and Lower Lake   | Facility (Parcels 16,19)                                   | Sediment                    |
|   | Establish natural stream channel flow and geomorphic conditions within Smelter reach  |  | Surface water               |
|   | Establish natural wetland/riparian conditions   |  | Sediment                    |
| Speiss Dross Slurry Wall  | Isolate impacted soil and prevent impacts to groundwater  |  | Groundwater                 |
| Source removals - Excavation and Removal of Impacted Media at Tito Park Area, former Acid Plant, and Upper Lake Marsh | Remove through excavation impacted soil/sediment that could potentially leach to groundwater or surface water                 | Facility (Parcels 16,19)                                   | Groundwater                 |
|   | Protectively manage removed soil under ET cover system  |  | Soil                        |
| CAMU 1 and CAMU 2   | Isolate impacted soil, sediment and remediation waste and prevent impacts to groundwater                                      | Facility (Parcels 16,19)                                   | Surface water               |
|   | Surface water/stormwater collection   |  | Sediment                    |
| Slag Pile - Grade and Cover   | ET Cover over unfumed slag to reduce infiltration   | Facility (Parcels 16,19)                                   | Groundwater                 |
|   | Slag pile regrading   |  | Soil/Slag                   |
|   | Surface water/stormwater collection   |  | Sediment                    |
| <b>INSTITUTIONAL CONTROLS IMPLEMENTED BY CUSTODIAL TRUST</b>  |   |  |                             |
| Custodial Trust Well Abandonment Program  | Contact all residents with existing supply wells; Abandon existing residential wells and/or provide alternative water supply  | Non Trust-Owned Properties                                 | Groundwater                 |
| Custodial Trust Deed Restrictions   | Implement deed restriction on Trust-owned property to restrict use to commercial/industrial only and prohibit groundwater use | Trust-Owned Properties including Facility (Parcels 16, 19) | Soil and Groundwater        |

**Table 6-1. Summary of Proposed Corrective Measures and Supplemental Institutional Controls**

*Corrective Measures Study Report, Former ASARCO East Helena Facility*

| Proposed Remedy Elements   | Engineering/Activity Components  | Applicable Parcels  | Applicable Media or Pathway |
|--|--|---|-----------------------------|
| <b>SUPPLEMENTAL INSTITUTIONAL CONTROLS IMPLEMENTED BY OTHERS</b> |  |   |                             |
| East Valley Controlled Groundwater Area (CGWA)                   | Implement and maintain program through CGWA process                              | CMS Parcels (including Facility),<br>Undeveloped Lands,<br>Non Trust-Owned Properties | Groundwater                 |
|  | Apply groundwater use restriction areas  |   |                             |
| City of East Helena Well Restrictions                            | Implement and maintain program through COEH process                              | CMS Parcels (including Facility),<br>Undeveloped Lands,<br>Non Trust-Owned Properties | Groundwater                 |
|  | Apply groundwater use restriction areas  |   |                             |
| Lewis and Clark County and City of East Helena Soil Ordinance    | Implement and maintain lead education and abatement program through COEH process | Non Trust-Owned Properties  | Soil                        |
|  | Apply property use restrictions  |   |                             |

Notes:

ET = evapotranspiration

PPC = Prickly Pear Creek

COEH = City of East Helena

Facility - Parcels 16, 19

CMS Parcels - Parcels 10, 11, 12, 15, 16, 17, 18, 19, 23, the portion of 8 located west of State Highway 518 (8W), and portions of Parcel 2 near Prickly Pear Creek (PPC; Parcel 2a)

Undeveloped Lands - Parcels 2, 3, 4, 6, 7, 9, 13, 14, the portion of 8 located east of State Highway 518 (8E), 21, and 22

Table 6-2. Summary of Remedy Performance Standards by Parcel  
 Corrective Measures Study Report, Former ASARCO East Helena Facility

| CMS Parcel                                  | Proposed Remedy   | Media with Potential Unacceptable Risk | Remedy Performance Standards   |  |  |   |
|---|---|--|--|--|--|---|
|   |   |  | Protect HH and Environment   | Achieve MCSs   | Control Sources  | Meets Current and Future Exposure/Use   |
| 2a  | Operable Unit 2 Record of Decision  | Soil                                   | No unacceptable risk (Table 4-1)   | To be evaluated upon transfer of property ownership  | Windborne deposition mitigated by ET Cover   | Currently land is undeveloped similar to Operable Unit 2 Record of Decision parcels             |
|   | South Plant Hydraulic Control and ET Cover  | Groundwater                            |  | Yes  | Interrelated IMs to reduce downgradient concentrations                             |   |
| 8W, 10, 11, 12, 17, 18                      | South Plant Hydraulic Control: Upper Lake and Lower Lake Removal, Prickly Pear Creek Bypass and Realignment, wetland construction | Soil                                   | No unacceptable risk (Table 4-1); IMs are reducing contaminant mass loadings and remedy is protective in combination with CGWA and COEH restrictions | Yes - contaminated soil and sediments were removed and replaced with clean materials                                       | N/A - sources removed  | Constructed riparian corridor appropriate for industrial (future) or recreational use (current) |
|   |   | Sediment                               |  |  |  |   |
|   |   | Surface water                          |  |  |  |   |
| 15  | Operable Unit 2 Record of Decision  | Soil                                   | No unacceptable risk (Table 4-1)   | To be evaluated upon transfer of property ownership  | Windborne deposition mitigated by ET Cover   | Meets industrial MCSs (future use); no risk to ecological receptors (current use)               |
|   | CGWA (supplemental institutional control implemented by others)   | Groundwater                            | Reduce potential for contact with and ingestion of impacted groundwater  | Contaminant concentrations are expected to decrease over time due to reductions in mass loading from remedy implementation | No source: plume in this area is attributed to naturally occurring arsenic         |   |
| 16, 19                                      | ET Cover, Source Removal, Speiss Dross Slurry Wall, CGWA (supplemental institutional control implemented by others)               | Soil                                   | - Prevent contact with impacted media through removal or under protective ET Cover   | Yes  | Removed or under protective ET Cover   | Meets industrial MCSs   |
|   |   | Groundwater                            |  |  |  |   |
|   | Grade and Cover   | Unfumed Slag                           | - Improve downgradient water quality over time   | Yes  | Reduce potential for slag and stormwater runoff to discharge in Prickly Pear Creek | Fumed slag available for recovery and industrial use  |
| 23  | Operable Unit 2 Record of Decision  | Soil                                   | No unacceptable risk (Table 4-1)   | Yes  | Windborne deposition mitigated by ET Cover   | Currently land is undeveloped similar to Operable Unit 2 Record of Decision parcels             |
| <b>Undeveloped Land</b>                     |   | <b>Exposure Media</b>                  | <b>Protect HH and Environment</b>  | <b>Achieve MCSs</b>  | <b>Control Sources</b>   | <b>Meets Current and Future Exposure/Use</b>  |
| 2, 3, 4, 6, 7, 9, 13, 14, 8E, 21, and 22    | Operable Unit 2 Record of Decision, COEH Soil Ordinance, COEH Well Restrictions   | Groundwater                            | Reduce potential for human contact with and ingestion of impacted groundwater  | Contaminant concentrations are expected to decrease over time due to reductions in mass loading from remedy implementation | Reduced concentrations at Facility will eventually propagate downgradient          | Ensures protection until groundwater meets MCSs   |
|   | Operable Unit 2 Record of Decision, COEH Soil Ordinance   | Soil                                   | Reduce potential for human contact with impacted soil  | MCS will be achieved by adherence to COEH soil ordinance or a Trust institutional control if not within COEH               | Windborne deposition mitigated by ET Cover   | Ensures property use is appropriate to existing conditions                                      |
| <b>Non-Custodial-Trust-Owned Properties</b> |   | <b>Exposure Media</b>                  | <b>Protect HH and Environment</b>  | <b>Achieve MCSs</b>  | <b>Control Sources</b>   | <b>Meets Current and Future Exposure/Use</b>  |
|   | Custodial Trust Well Abandonment Program; COEH Well Restrictions; CGWA (supplemental institutional control implemented by others) | Groundwater                            | Reduce potential for human contact with and ingestion of impacted groundwater  | Contaminant concentrations are expected to decrease over time due to reductions in mass loading from remedy implementation | Reduced concentrations at Facility will eventually propagate downgradient          | Ensures protection until groundwater meets MCSs   |
|   | Operable Unit 2 Record of Decision, COEH Soil Ordinance   | Soil                                   | Reduce potential for human contact with impacted soil  | MCS will be achieved by adherence to COEH soil ordinance or a Trust institutional control if not within COEH               | Windborne deposition mitigated by ET Cover   | Ensures property use is appropriate to existing conditions                                      |

Notes:

8E = the portion of parcel 8 located east of Highway 518

8W = the portion of parcel 8 located west of Highway 518

CGWA = Controlled Groundwater Area (supplemental institutional control implemented by others)

COEH = City of East Helena

ET = evapotranspiration

IM = interim measure

MCS = media cleanup standard

NA = not applicable



Table 6-3. Preliminary Summary of Performance Monitoring Requirements

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| Proposed Remedy Elements   | Engineering/Activity Components  | Applicable Media or Pathway | Remedial Objectives  | Performance Monitoring Requirements                          |  |
|--|--|-----------------------------|--|--|--|
|  |  |                             |  | Monitoring (Media)   | Engineering Components Monitoring                                      |
| <b>ENGINEERING CONTROLS</b>  |  |                             |  |  |  |
| Slag Pile - Grade and Cover  | ET Cover over unfumed slag to reduce infiltration  | Groundwater                 | - Reduce infiltration through unfumed Slag and subsequent leaching of metals from unfumed Slag   | CAMP Program (Groundwater)                                   | Cover Inspections and Maintenance                                      |
|  | Slag pile regrading  | Soil/Slag<br>Sediment       | - Maintain access to slag for sale<br>- Reduce potential for slag discharge to Prickly Pear Creek  | Slag pile slope grading plan                                 | Slope inspections and comparison to design parameters                  |
|  | Surface water/stormwater collection  | Surface water               | - Reduce potential for slag and stormwater runoff from discharging to Prickly Pear Creek   | CAMP Program (Surface Water)                                 | Cover Inspections and Maintenance                                      |
| ET Cover System - Building Demolition, Utility Abandonment, Subgrade Fill, Final ET Cover  | ET Cover to mitigate infiltration of precipitation, control wind erosion   | Groundwater                 | - Reduce infiltration of precipitation through impacted soil to groundwater<br>- Eliminate uncontrolled water collection and discharge to groundwater through buried utilities<br>- Improve Site and down-gradient groundwater quality | CAMP Program (Groundwater)                                   | Cover Inspections and Maintenance                                      |
|  |  | Soil<br>Sediment            | - Reduce potential for direct contact of impacted media with human and ecological receptors  | Not Applicable   |  |
|  | Surface water/stormwater collection  | Surface water               | - Reduce volume of stormwater and prevent stormwater contact with impacted media   | CAMP Program (Surface Water)                                 |  |
| South Plant Hydraulic Controls: Upper Lake and Lower Lake Removal; PPC Bypass; PPC Realignment; wetland construction                 | Reduce surface water loading to groundwater by removing Upper Lake and Lower Lake  | Groundwater                 | - Lower groundwater table to reduce groundwater contact with impacted subsurface soil<br>- Reduce offsite flux   | CAMP Program (Groundwater)                                   | Not applicable   |
|  | Establish natural stream channel flow and geomorphic conditions within Smelter reach   | Surface water               | - Improve surface water quality of PPC by reducing loading from tributary sources  | CAMP Program (Surface Water)                                 |  |
|  | Establish natural wetland/riparian conditions  | Sediment                    | - Reduce impacted sediment discharge to PPC within Smelter reach<br>- Prevent flooding   | Not Applicable   |  |
| Source removals - Excavation and Removal of Impacted Media at Tito Park Area, Acid Plant, Upper Lake Marsh, and Speiss Disposal Area | Remove through excavation impacted soil/sediment that could potentially leach to groundwater or surface water                | Groundwater                 | - Improve localized groundwater conditions within removal areas<br>- Improve down-gradient groundwater quality   | CAMP Program (Groundwater)                                   | Not applicable (see ET Cover System)                                   |
|  |  | Soil                        | - Reduce potential for human contact with impacted soil  | Not Applicable   |  |
|  | Protectively manage removed soil under ET cover system   | Surface water<br>Sediment   | - Improve surface water quality of PPC by reduced loading from tributary sources<br>- Reduce impacted sediment discharge to PPC within Smelter reach   | CAMP Program (Surface Water)<br>Not Applicable               |  |
| Speiss Dross Slurry Wall   | Isolate impacted soil and prevent impacts to groundwater   | Groundwater                 | - Improve localized groundwater conditions outside of slurry wall area<br>- Improve down-gradient groundwater quality  | CAMP Program (Groundwater)                                   | Not applicable   |
| <b>INSTITUTIONAL CONTROLS (ICs)</b>  |  |                             |  |  |  |
| Custodial Trust Well Abandonment Program   | Contact all residents with existing supply wells; Abandon existing residential wells and/or provide alternative water supply | Groundwater                 | - Reduce potential for human contact with and ingestion of impacted groundwater  | Verification of Alternative Water Supply or Treatment System | Formally confirm all residents with existing supply wells are notified |
| <b>SUPPLEMENTAL ICs IMPLEMENTED BY OTHERS</b>  |  |                             |  |  |  |
| Controlled Groundwater Area (CGWA)   | Implement and maintain program through CGWA process<br>Apply groundwater use restriction areas                               | Groundwater                 | - Reduce potential for human contact with and ingestion of impacted groundwater  | CAMP Program (Groundwater)                                   | Maintain CGWA program until conditions are met                         |
| COEH Well Restrictions   | Implement and maintain program through COEH process<br>Apply groundwater use restriction areas                               | Groundwater                 | - Reduce potential for human contact with and ingestion of impacted groundwater  | CAMP Program (Groundwater)                                   | Monitored through COEH program   |
| COEH Soil Ordinance  | Implement and maintain program through COEH process<br>Apply property use restrictions                                       | Soil                        | - Reduce potential for human contact with impacted soil<br>- Ensure that property use is appropriate to existing conditions  | Not Applicable   | Monitored through COEH LEAP program                                    |